

# Design Study Update 

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## 1) Design With Stages Downstream the light path



## 2) OSM UNITS WELDED STRUCTURE



## 3) LOWFS ASSY BOLTED STRUCTURE


4) LOWFS ASSY INTEGRATION


## 5) Restricting the Optical Equation: : a = b Should be the same for each OSM

Consequence: The length of the lever arm is now the variable!


Optical Layout (Fig. 3) is optimized when the following equations are verified:
5.1) $a=b \& c=d$
5.2) $a+b=x(c+d)$

Keeping the AO Focus away from the Probe mirror (FM1) gives:
5.3) $a=a_{1}+a_{2}$

Keeping each Lever arms on a different plane to avoid collision between each other gives a different value of a1 for each OSM
The Lever Arm Length previously determined gives:
5.4) Lever Arm length $=\mathrm{b}+\mathrm{a}_{2}$

Replacing 3.3 \& 3.4 in 3.1 gives: $a=b \rightarrow a_{1}+a_{2}=$ Lever Arm length $-a_{2}$
Solving for $\mathrm{a}_{2} \rightarrow 2 \mathrm{a}_{2}=$ Lever Arm length $-\mathrm{a}_{1} \rightarrow \mathrm{a}_{2}=\left(\right.$ Lever Arm length $\left.-\mathrm{a}_{1}\right) / 2$

## 6) Sizing the Probe

6.1) Probe FoV size depends directly from it's distance from the Focal plane.

The probe Fold Mirror intercept the light beam at a 45 degree angle creating an elliptical projection at a distance a1 from the Focal plane.
The minimum diameter of the mirror needs to be larger than the Ellipse Major Diameter. The Larger Fold mirror will be at the furthest distance from the Focal plane OSM \#1 (a1 = -20)

Each Probe FoV is a potential vignetting of an other probe.
6.1.1) Largest FoV at the Fold Mirror \#1 (FM1) is at OSM \#1 (a1 = -20) Probe

> Ellipse Minor Diameter: $\begin{aligned} \mathrm{d} & =\mathrm{d} \text { at Focus Plan + (a1 / f\# }) \\ & =5 \times 0.727+(20 / 13.66) \\ & =3.635+1.464 \\ \mathrm{~d} & =5.10 \mathrm{~mm}\end{aligned}$

$$
\begin{aligned}
& \text { Ellipse Major Diameter: } \\
& D=d \sqrt{ } 2=5.1 \sqrt{ } 2 \\
& D=7.21 \mathrm{~mm}
\end{aligned}
$$

FM1

Probe

6.1.2) Smallest FoV at the Fold Mirror \#1 (FM1) is at OSM \#2 (a1 = -5) Probe

Ellipse Minor Diameter:

$$
\begin{aligned}
\mathrm{d} & =\mathrm{d} \text { at Focus Plan }+(\mathrm{a} 1 / \mathrm{f} \#) \\
& =5 \times 0.727+(5 / 13.66) \\
& =3.635+.366 \\
\mathrm{~d} & =4.00 \mathrm{~mm}
\end{aligned}
$$

$$
\begin{aligned}
& \text { Ellipse Major Diameter: } \\
& D=d \sqrt{ } 2=4 \sqrt{ } 2 \\
& D=5.66 \mathrm{~mm}
\end{aligned}
$$

6.1.3) Medium FoV at the Fold Mirror \#1 (FM1) is at OSM \#3 (a1 = 10) Probe

Ellipse Minor Diameter:
$\mathrm{d}=\mathrm{d}$ at Focus Plan $+(\mathrm{a} 1 / \mathrm{f} \#)$
$=5 \times 0.727+(10 / 13.66)$
$=3.635+.732$
$\mathrm{d}=4.37 \mathrm{~mm}$

Ellipse Major Diameter:
$\mathrm{D}=\mathrm{d} \sqrt{ } 2=4.37 \sqrt{ } 2$
$\mathrm{D}=6.18 \mathrm{~mm}$

Choosing to standardize to an 8 mmDiameter Mirror for each probe would facilitate manufacturing (Similar probe size, etc...) and purchasing, but would adversely increase the vignetting.

IS IT ACCEPTABLE?
6.2) Minimum Probe length:

The probe needs to be long enough to extend through the 120 " Diameter FoV without vignetting any other portion of the FoV.

The smallest probe is OSM \#3 (a1 = 10)
Then, using OSM \#3, $a_{2}$ must be at least 120 mm

$$
\begin{aligned}
& \text { (Eq. 5.3) } \rightarrow \mathrm{a}=\mathrm{a}_{1}+\mathrm{a}_{2}=20+120=130 \\
& \text { (Eq. 5.1) } \rightarrow \mathrm{a}=\mathrm{b}
\end{aligned}
$$

With $\mathrm{a}=\mathrm{b}=130$ and:

OSM \#1 $\rightarrow \mathrm{a} 1=-20 \mathrm{~mm} \rightarrow \mathrm{a}_{2}=\mathrm{a}-\mathrm{a}_{1}=130--20=150$
OSM \#2 $\rightarrow \mathrm{a} 1=-5 \mathrm{~mm} \rightarrow \mathrm{a}_{2}=\mathrm{a}-\mathrm{a}_{1}=130--5=135$
OSM \#3 $\rightarrow \mathrm{a} 1=10 \mathrm{~mm} \rightarrow \mathrm{a}_{2}=\mathrm{a}-\mathrm{a}_{1}=130-10=120$
Lever Arm length $=\mathrm{b}+\mathrm{a}_{2}$ (Eq. 5.4)
OSM \#1 Lever Arm Length $=\mathrm{b}+\mathrm{a}_{2}=130+150=280$
OSM \#2 Lever Arm Length $=b+a_{2}=130+135=265$
OSM \#3 Lever Arm Length $=b+a_{2}=130+120=250$

## 6.3) Light Beam Dimension

| OSM\# | $\mathrm{a}_{1}$ | $\mathrm{a}=\mathrm{b}$ | $\mathrm{a}_{2}=\mathrm{a}-\mathrm{a}_{1}$ | Arm $=\mathrm{b}+\mathrm{a}_{2}$ |
| :---: | :---: | :---: | :---: | :---: |
| I | -20 | 130 | 135 | 280 |
| II | -5 | 130 | 142.5 | 265 |
| III | 10 | 130 | 150 | 250 |


6.4) Probe Arm Length

OSM \#1


OSM \#2


OSM \#3


## 6.4) Design Features Common to all Probes



- Probe Cross Section

- Fold Mirror
6.5) Frequency Analysis

OSM \#1

| List Modes |  |  |  | 区 |
| :---: | :---: | :---: | :---: | :---: |
| Study name: Frequency |  |  |  |  |
| Mode No. | Frequency(Rad/sec) | Frequency(Hertz) | Period(Seconds) |  |
| 1 | 1480.3 | 235.59 | 0.0042446 |  |
| 2 | 2512 | 399.79 | 0.0025013 |  |
| 3 | 9407 | 1497.2 | 0.00066792 |  |
| 4 | 15592 | 2481.6 | 0.00040296 |  |
| 5 | 25594 | 4073.5 | 0.00024549 |  |
| $\leqslant$ |  |  |  | 7 |
| Close |  | Save | Help |  |



OSM \#2


OSM \#3

6.6) Probe Deflection, at rest, under it's own weight:

- Deflection analyzed on the longest Inclined probe (OSM \#2)



Probe Deflection

- Mass of the probe $w=m g=0.01 \mathrm{Kg} \times 9.81 \mathrm{~ms}^{-2}=0.098 \mathrm{~N}$
-Moment of Inertia: $\mathrm{I}=\mathrm{bh}^{3} / 12=4.57 \times 7.64^{3} / 12=169.8 \mathrm{~mm}^{4}$
-6061-T6 Module of Elasticity: $\mathrm{E}=68,800 \mathrm{~N} / \mathrm{mm}^{2}$
-Max Deflection: $v=w L^{3} / 8 E I$
$v=0.098 \times 100^{3} /(8 \times 68,800 \times 169.8)$
$v=98000 / 93457920$


Probe Length
$\mathrm{v}=0.001 \mathrm{~mm}$

## Remaining work to be done

-System rigidity Analysis

## Questions:

-Probe position Accuracy: 40 (KAON 562) or 70 mas (Contour)

- Minimum Incremental motion ?
- Max Wobble?
- Position Stability (5 mas / 3600 s) TBC
- TT Requirements (Deflection, response, resolution,...)

