

## Design Study Update

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## 1. Conceptual design and operation

Three probes cover the entire Ø 120" (87.24 mm) Field of View.

Each probe is mounted on a 2 degrees of freedom articulated arm composed of a crank arm and a lever arm, driven by 2 corresponding rotation motors: The crank and lever motors. (See Fig. 2)

Any position in the OSM field of view can be acquired by calculating appropriate values for theta and phi, noting that two possible solutions could be found due to symmetry.

The crank motor is secured to the Sensor and rotates the crank arm, precisely about the rotation axis of the crank motor referred to as the theta axis. The lever arm motor provides the necessary second degree of freedom by rotating the lever arm and all associated optics, about the phi axis.

Each probes are a at a different distance from the Focal plane, 15mm apart, with the closest probe 5 mm upstream from the focal plane. This design allow each probe to freely roam the entire field without risk of colliding into an other probe. (See Fig. 1)

# Focal Plane OSM #3 Fig. 1

#### 1.1 Basic Design requirements:

|  | Mechanism Type:   | φ/θ                  |  |  |
|--|---|----------------------|--|--|
|  | Patrolled Field:  | Ø 120" (87.24mm)     |  |  |
|  | Focal Plane FoV :   | Ø 5" (3.635mm)       |  |  |
|  | Acquisition accuracy: 40 mas (30µm)                                     |                      |  |  |
|  | Stability:  | 5 mas / 3600s (1 μm) |  |  |
|  | Position knowledge:   | < 1 μm (TBC)         |  |  |
|  | Minimum Incremental motion: TBD<br>Operating Temperature: -10°C +/- 0.3 |                      |  |  |
|  |   |                      |  |  |

#### 1.2 Field of View:

The Field of View at the Focal Plane is  $\emptyset$  5" (3.635mm)

The Field of View at the probe is defined by it's distance from the Focal Plane / f# (See Fig. 2)





## 2. Optical Equation



Optical Layout (Fig. 3) is optimized when the following equations are verified:

2.1) a = b = c = d

2.2) a + b = x (c + d)

Keeping the AO Focus away from the Probe mirror (FM1) gives:

2.3)  $a = a_1 + a_2$ 

Keeping each Lever arms on a different plane to avoid collision between each other gives a different value of a1 for each OSM The Lever Arm Length previously determined gives:

2.4) Lever Arm length =  $b + a_2$ Replacing 3.3 & 3.4 in 3.1 gives:  $a = b \rightarrow a_1 + a_2 = \text{Lever Arm length} - a_2$ Solving for  $a_2 \rightarrow 2a_2 = \text{Lever Arm length} - a_1 \rightarrow a_2 = (\text{Lever Arm length} - a_1)/2$ 

### 3. Dimensioning the Probe

(3.1) The Lens Holder size is driving  $a_2$ 

#### 3.2) Using a 280mm Lever Arm:

a1 = 10 mm for OSM #1  $\rightarrow$  10 + 2a<sub>2</sub> = 280  $\rightarrow$  2a<sub>2</sub> = 280 - 10  $\rightarrow$  a<sub>2</sub> = 135 a1 = -5 mm for OSM #2  $\rightarrow$  -5 + 2a<sub>2</sub> = 280  $\rightarrow$  2a<sub>2</sub> = 280 + 5  $\rightarrow$  a<sub>2</sub> = 142.5 a1 = -20 mm for OSM #3  $\rightarrow$  -20 + 2a<sub>2</sub> = 280  $\rightarrow$  2a<sub>2</sub> = 280 + 20  $\rightarrow$  a<sub>2</sub> = 150

| OSM# | a <sub>1</sub> | a <sub>2</sub> | $a = b = a_1 + a_2$ | a+b |
|------|----------------|----------------|---------------------|-----|
| I    | 10             | 135            | 145                 | 240 |
| II   | -5             | 142.5          | 137.5               | 275 |
| III  | -20            | 150            | 130                 | 260 |



#### 3.3) Probe Collision avoidance



## Design With Stages Upstream the light path



## LOWFS OSM Assy with stages upstream



## Remaining work to be done

-Analyze Tip/Tilt Mirror Vibrations and Impact on Probe stabilization.

- System rigidity Analysis

## Questions:

-Probe position Accuracy: 40 (KAON 562) or 70 mas (Contour)

- Minimum Incremental motion ?
- Max Wobble?
- Position Stability (5 mas / 3600 s) TBC
- TT Requirements (Deflection, response, resolution,...)