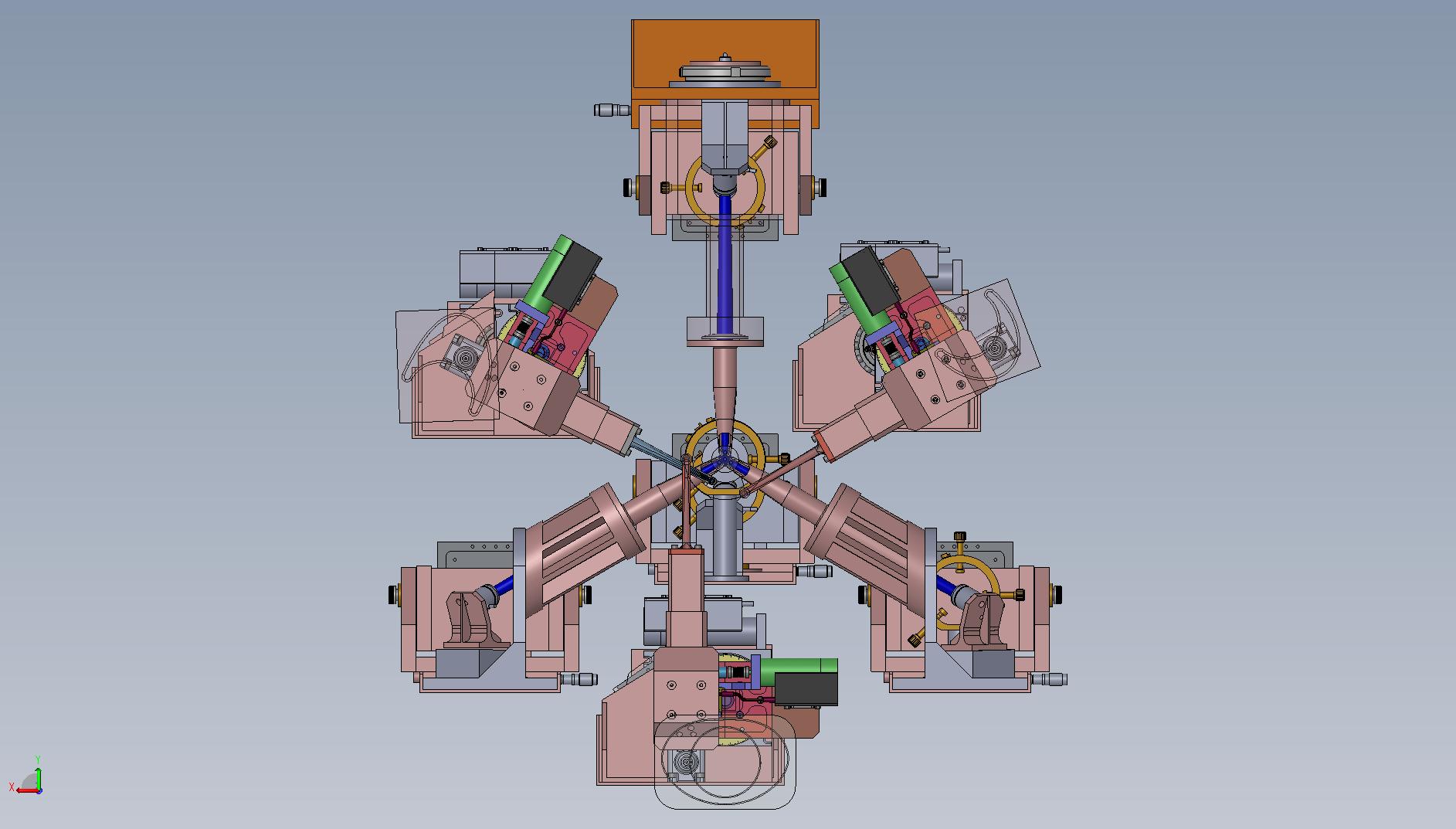
LGS Wavefront sensor sub-system preliminary design

## KECK ADAPTIVE OPTICS NOTE xxx



# Introduction and Overview of concept

This document describes the preliminary design of the Laser Guide Star Wavefront Sensors (LGSWFS) for Keck’s Next Generation Adaptive Optics (NGAO) system.

Following the conceptual design review a Build-to-Cost (B2C) review was conducted which led to considerable changes in the system architecture, in particular to the LGS WFS architecture[[1]](#endnote-1). Firstly, the deployable quincunx asterism was de-scoped to a fixed LGS asterism with one on-axis LGS and three fixed symmetrically located LGS’s located at 10” radius. The FoV of the three movable PnS LGS used to sharpen the NGS TT stars was reduced from 150” to 120”. To further simplify the architecture and ease implementation, the wavefront measurements from these TT stars and the corresponding LGS WFS will be used to run separate AO systems that sharpen the TT stars but don’t contribute to the tomographic reconstruction.

Another significant change is the implementation of the LGS differential TT on the downlink rather than stabilize the laser beacon on sky. This provides for better control bandwidth as the time-delay between a measurement and TT correction is much smaller by the cycle time of light traveling up and down to the sodium layer.

The LGSWFS team has tried to design a simple, cheap and transmission efficient system that fulfills the requirements.

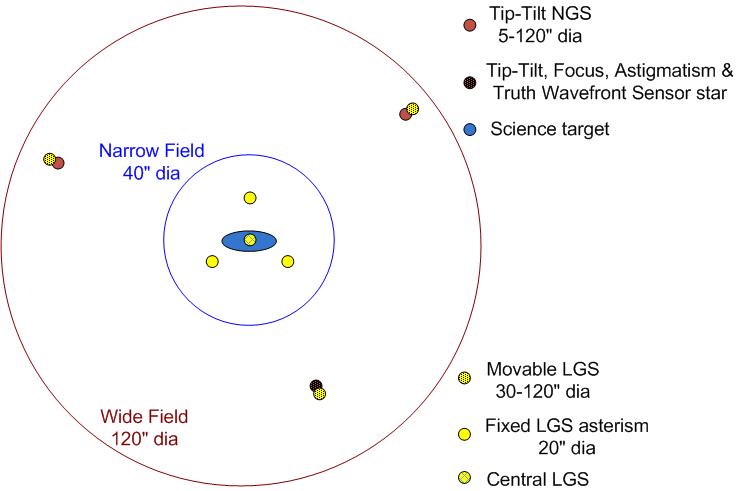


Figure - LGS “3+1” tomography asterism for the science field and three point and shoot lasers for image sharpening of the tip-tilt stars

# Context diagram



Figure - Context diagram of the LGSWFS showing the basic mechanical, optical and control interfaces to the AO system

is a basic context diagram of the LGSWFS assembly showing the interfaces of the WFS subsystem with rest of the NGAO system. LGSWFS make centroid measurements using 589 nm light from the AO system and send this data to the RTC to drive the LODM, HODM the 32x32 actuator MEMS DM’s in the TT(FA) WFS channels. At the same time the RTC also controls the downlink TT mirror position. The supervisory control computer helps deploy the PnS sensors and acquire the LGS light and configure the LGSWFS cameras (bias levels, gains, frame rate etc.). The LGSWFS subsystem will provide a status signal to the supervisory computer as a status monitor. shows a more detailed schematic of the LGSWFS assembly. Shown in the figure are a single PnS WFS channel with a deployable theta-phi pick-off mechanism with a fast downlink TT mirror, a slow TT mirror to register the lenslet and HODM pupils at each point in the field of regard and a rotary mechanism that rotates the WFS channel to keep the orientation of the lenslet and HODM acutators constant by undoing rotation introduced by the theta-phi mechanism.

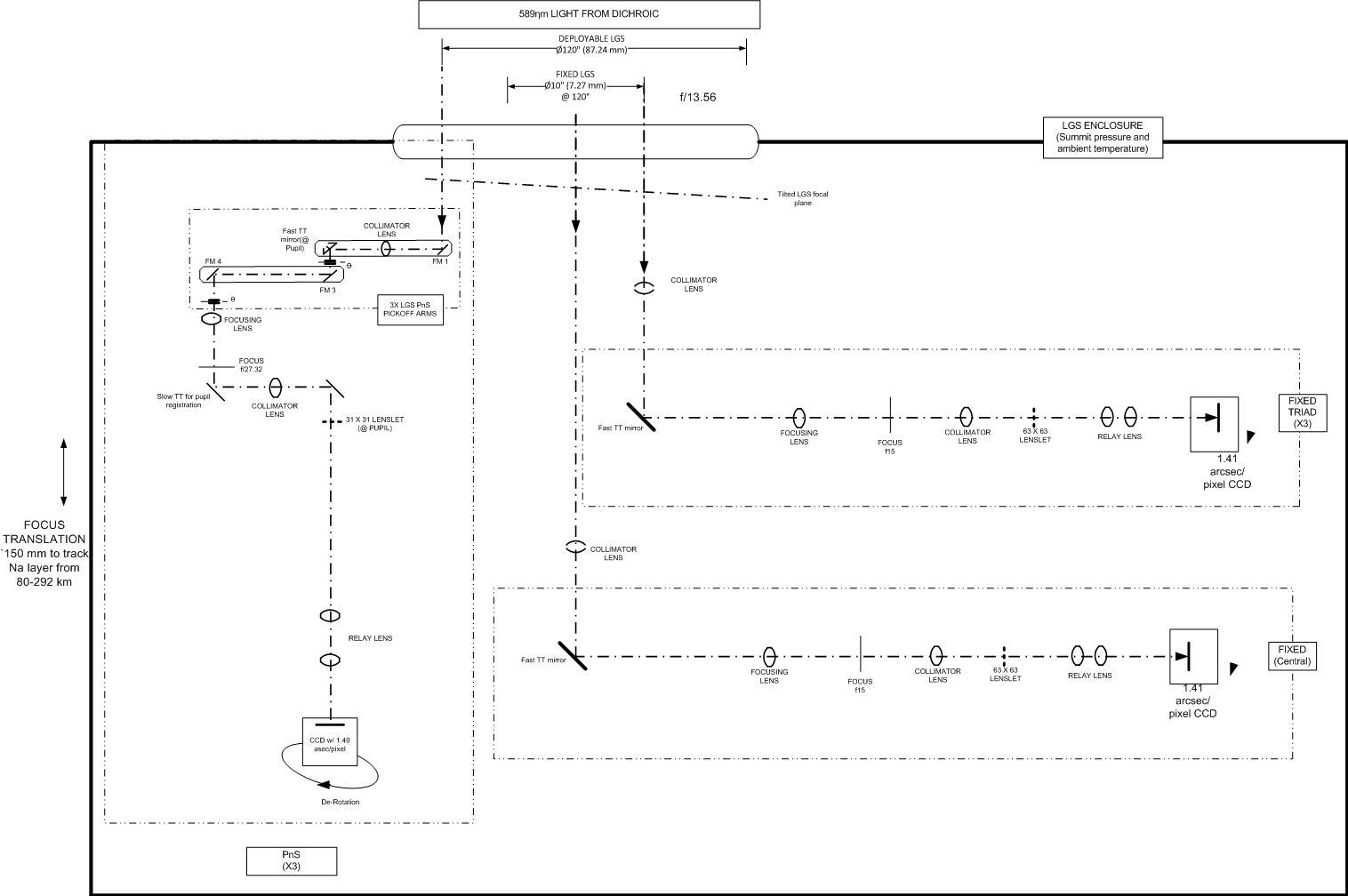


Figure - Schematic of the LGSWFS assembly showing a PnS WFS channel with pick off and TT mirrors and the central and one arm of the tomo. LGSWFS’s.

# Reference documents

* 1. [KAON 551 Wavefront Sensor System Conceptual Design Report](http://www.oir.caltech.edu/twiki_oir/pub/Keck/NGAO/AOSystemDesign/WFS_design_report_rev5.pdf)
  2. [511 System Design Manual v2.1 (doc)](http://www.oir.caltech.edu/twiki_oir/pub/Keck/NGAO/NewKAONs/KAON511_NGAO_SDM_v2.1.doc), dated March 30th, 2008
  3. [Preliminary Design Manual](http://www.oir.caltech.edu/twiki_oir/pub/Keck/NGAO/NewKAONs/KAON_NGAO_PDM_v0.3.doc) (as of November 12th, 2009)
  4. [685 Opto-mechanical Design Document](http://www.oir.caltech.edu/twiki_oir/bin/viewfile/Keck/NGAO/NewKAONs?rev=2;filename=PDR_AOrelay_design_v4.pdf)
  5. [666 Fixed Pupil Mode](http://www.oir.caltech.edu/twiki_oir/pub/Keck/NGAO/NewKAONs/KAON666_NGAO_Fixed_Pupil_Mode.doc)
  6. [Flowdown Error Budget](http://www.oir.caltech.edu/twiki_oir/pub/Keck/NGAO/FlowdownSummary/NGAO_PD_Phase_Flowdown_Budgets_v0_96_2003_Format.xls)

# AO relay path to LGSWFS input

The Laser guide star light path is shown in , the laser light traverses through the K mirror and the fold followed by the 1st AO relay OAP, after which it is incident on the DM. Following the DM it is folded by a notch dichroic and a 1m focal length plano-convex lens, with the convex surface being a parabola, focuses the beam to a tilted focal plane. The Laser Guide Star Wavefront Sensor assembly is located after the focus created by the AO relay. shows the mechanical layout of the NGAO system indicating the location of the LGSWFS assembly.

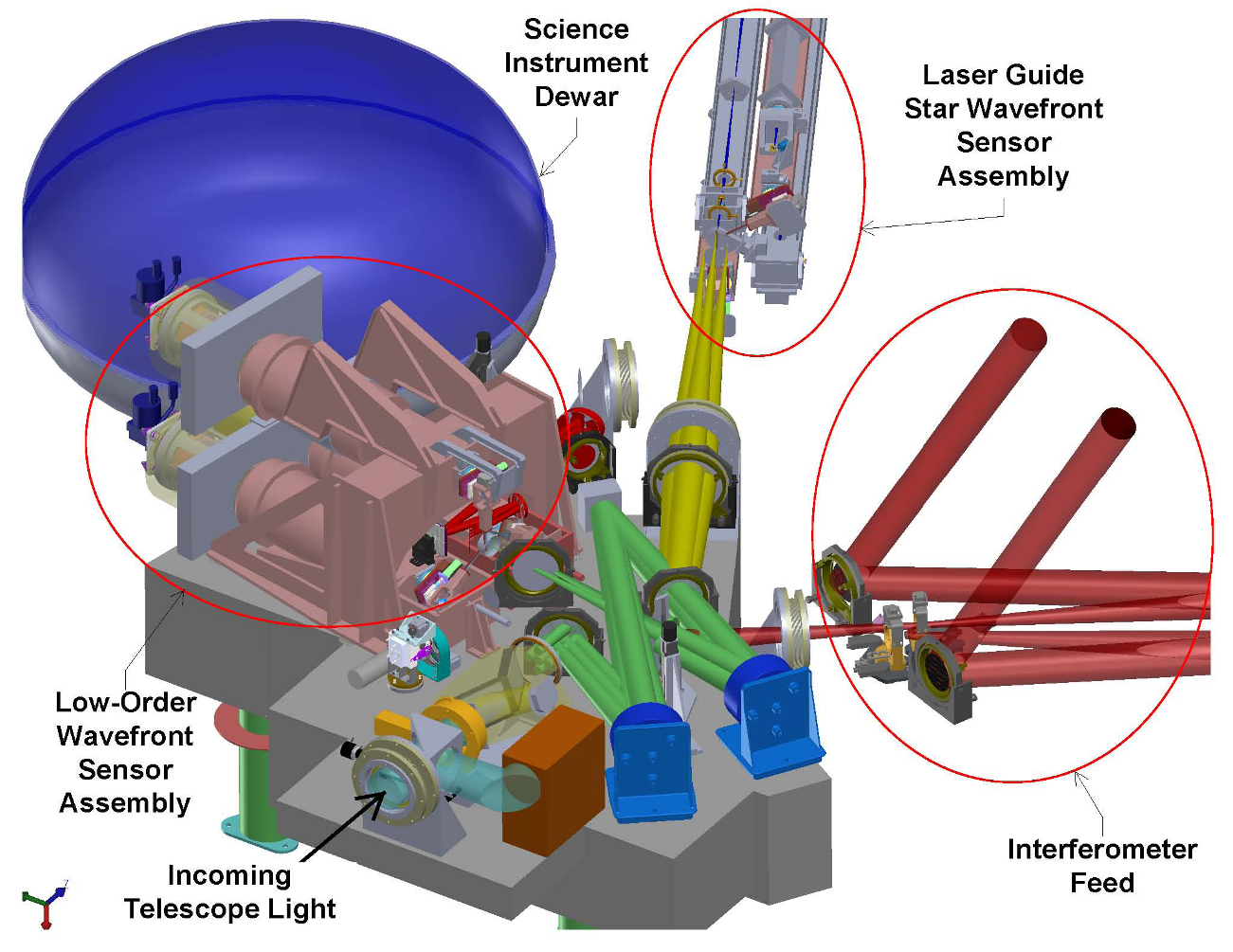


Figure - NGAO optical layout showing the location of the LGSWFS assembly WRT rest of the system (pic. courtesy C. Lockwood, UCO Lick)

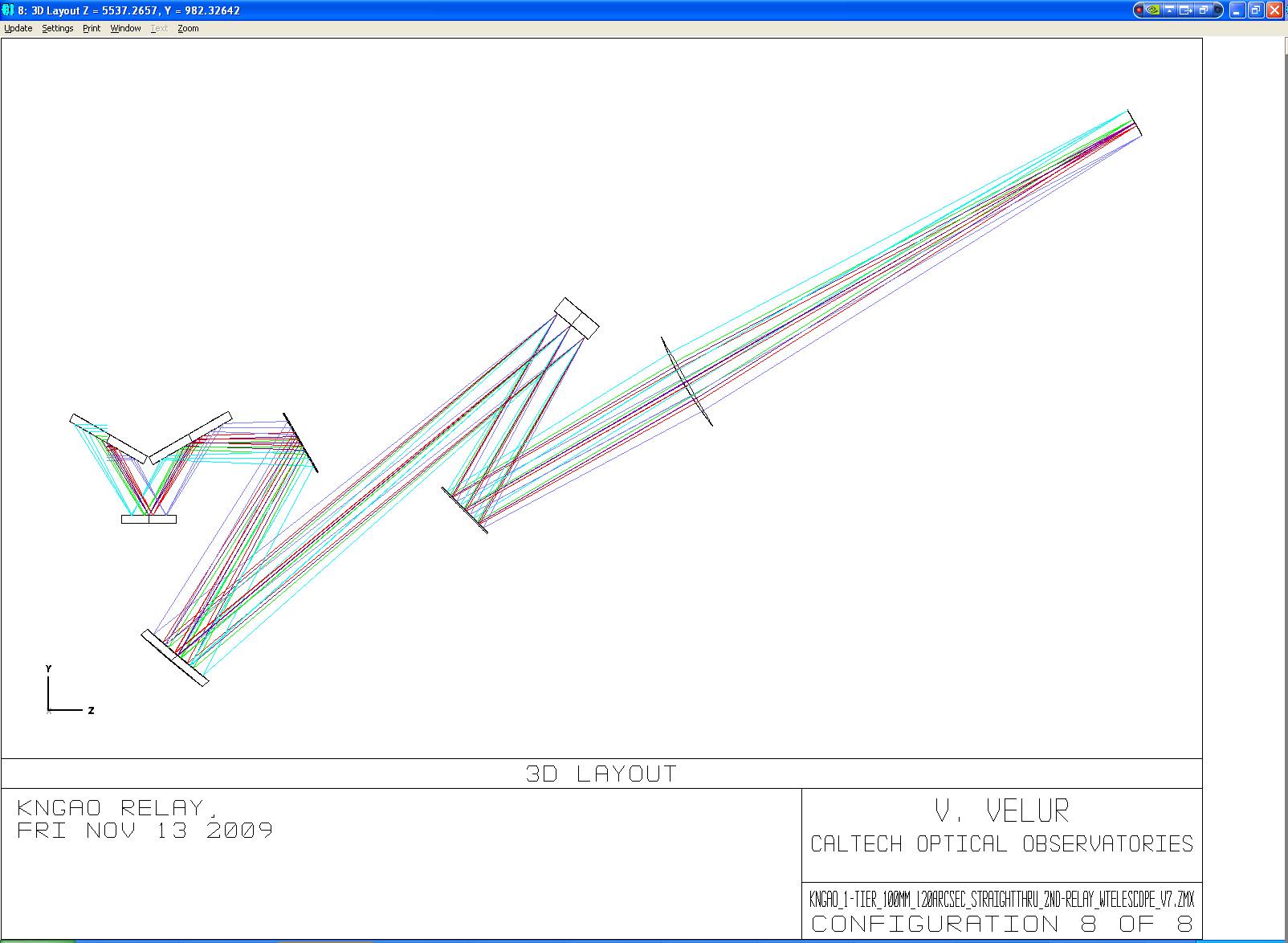


Figure - Laser guide star light path starting from the K mirror to the LGSWFS pick-off focal plane.

shows the spot diagram from the AO relay at 90 Km Na layer distance. The central fixed LGS spots delivered by the AO relay have RMS radii between 25 and 45 um at the LGS pick-off plane. The PnS LGS spots sizes range between 130 and 150 um RMS radius. The working F# at the LGS pick-off is 13.56 at 22 degrees off zenith and 720 um at the LGS pick-off plane corresponds to an arcsec on sky as per Zemax model of the NGAO Optical Relay. It is useful to note that the LGS focal plane delivered by the AO system is both curved and tilted. The curvature of the focal plane varies between 883 mm and 2604 mm as the distance to Na-layer varies from 90 to 180 Km.

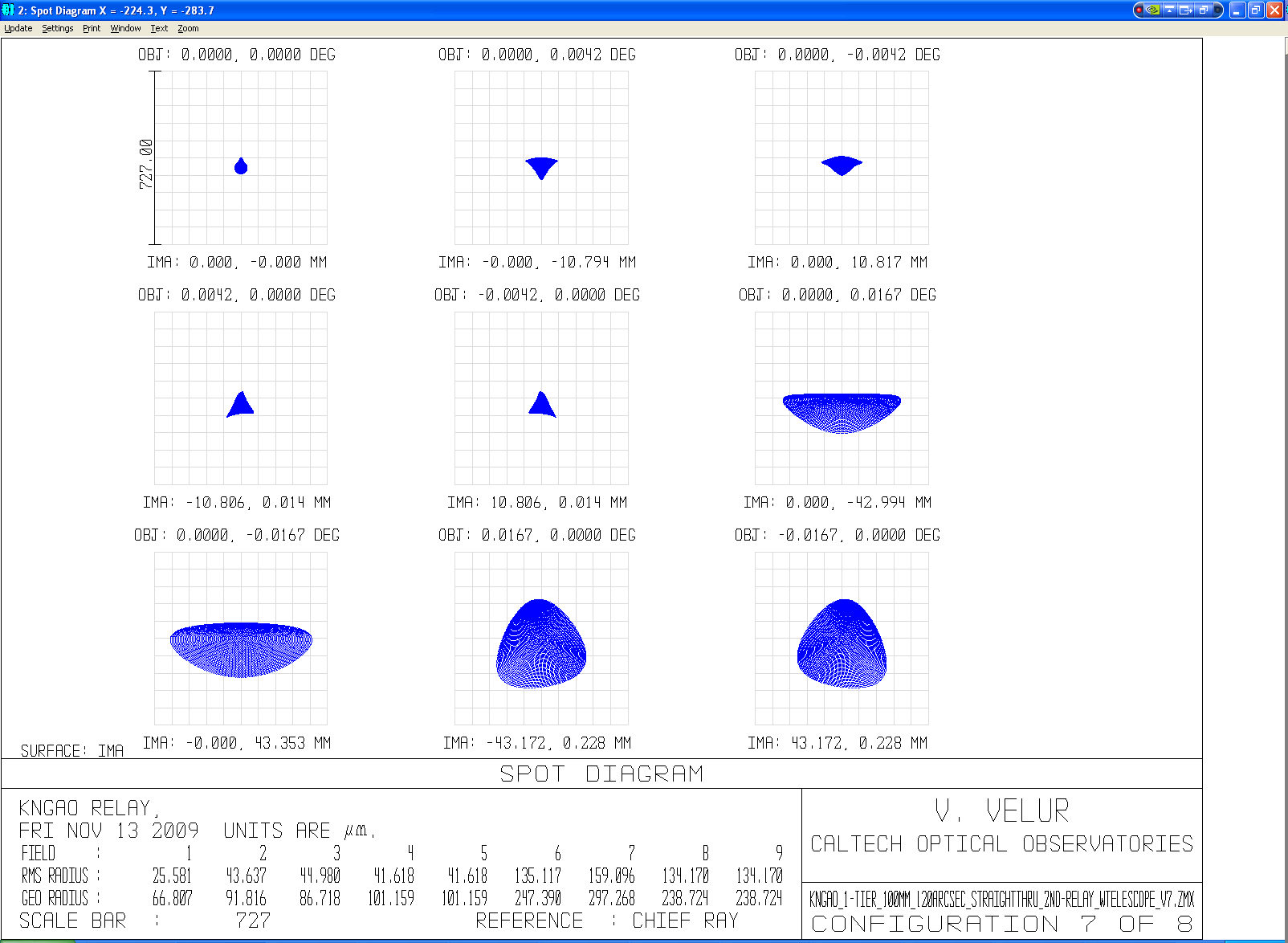


Figure - LGSWFS spots when the telescope is pointing at zenith. The fixed LGS spots at the LGSWFS pick-off focal plane is 25-45 um (RMS) radius while the PnS LGSWFS spots are as big as 160 um (RMS) at the edge of the field.

To understand the effect rather large spot sizes delivered by the AO relay as seen by the most affected PnS LGS WFS sub-apertures, we swap the Keck primary mirror with movable aperture that is 1/31st of the primary mirror and de-center this aperture to the extreme points of the primary mirror to look at the resulting spots to understand what happens at the Shack-Hartmann sub-apertures. One can see RMS radii of almost 6 um at the edge of the field as is shown by and .

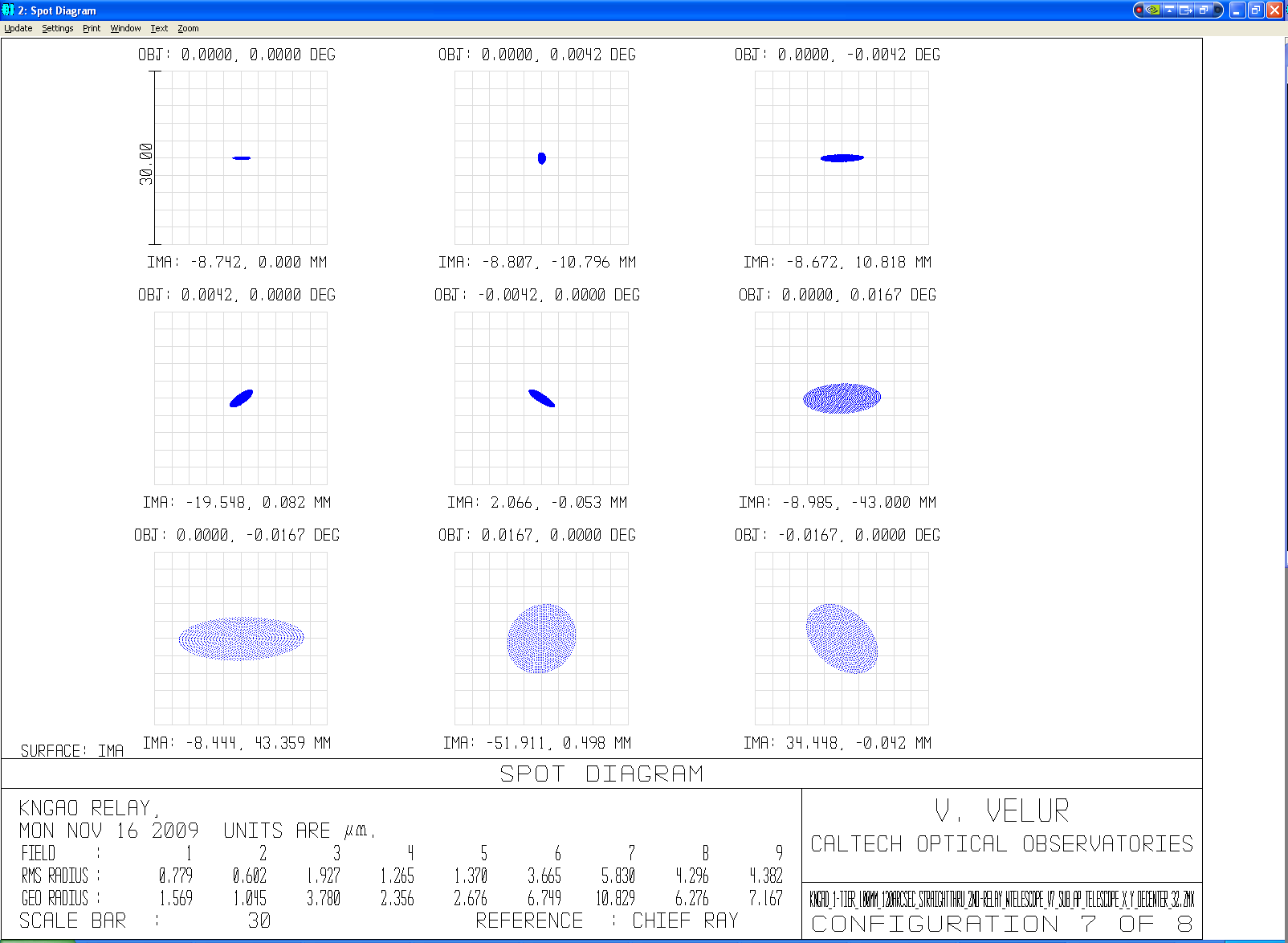


Figure LGS spots as seen by a single PnS LGSWFS sub-aperture. The spots diagram was generated by creating a de-centered aperture that is 1/31st the size of the Keck primary mirror and making the entrance pupil the size of a single sub-aperture. The aperture parameter in the Surface Property Menu was set to the primary mirror radius (5297.9 mm) to accommodate ray tracing. The worst case sub-aperture spots see a 6 um (RMS) radius.

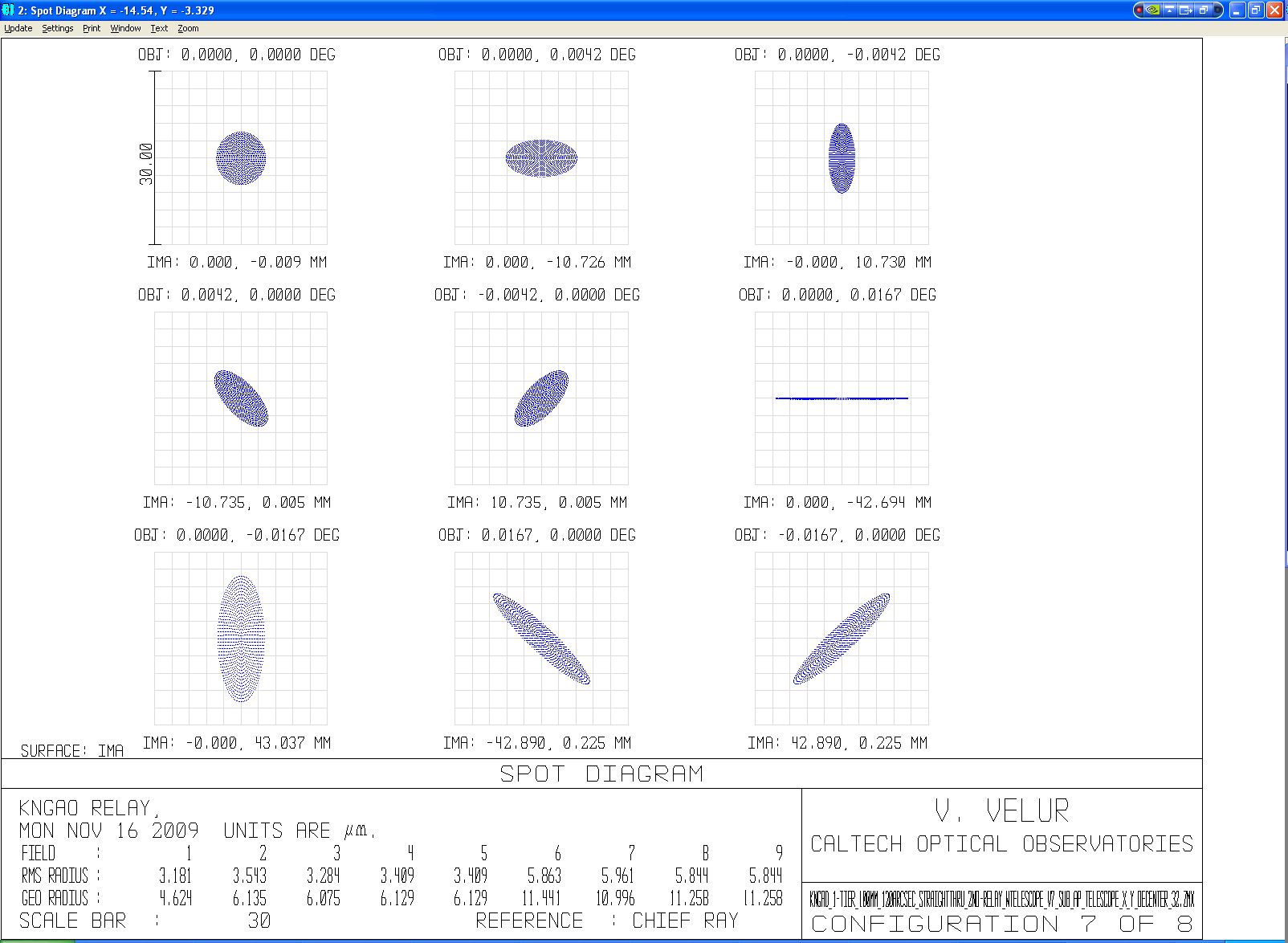


Figure - LGS spots as seen by a PnS LGSWFS sub-aperture (de-centered in the orthogonal direction). Worst case sub-apertures are 6 um (RMS) radius.

# Requirements highlights

# WFS Design

## Relevant analysis for design

### Pixel scale choice

From experience we know that characterizing and calibrating each sub-aperture of the 7 WFS for non-linearity is non-trivial and hence we choose the plate-scale to ensure that the sensor operates in its linear regime. Pixel scale is chosen based on the apparent spot size (sans charge diffusion). , extracted from the EBS, shows the apparent spot size for the tomographic (left column) and PnS (right column). For the fixed LGS asterism, the 1D tilt error is 50 mas and the diffraction limited sub-ap spot size is 699 mas, so we choose p=0.5 from to accommodate capture range and linear operating regime. For the variable asterism the 1D tilt error is 329 mas and the sub-ap diffraction limited spot size is 343 mas, so we choose P=1.0 for this sensor based on to be able to measure +/-2.5 waves of tilt.

|  |  |  |  |
| --- | --- | --- | --- |
| Detector size per subaperture | Pixel Size/ spot size (p) | Useful tilt range +/- waves | Departure from linearity |
| 2x2 | 1.0-1.5 | 0.5 | 0.024 |
| 2x2 |  | 1.0\* | .13\* |
| **4x4** | **0.5** | **1.5** | **0.019** |
| 4x4 | 0.67 | 2 | 0.085 |
| **4x4** | **1** | **2.5** | **0.19** |
|  |  |  |  |
| \* - nonlinear response |  |  |  |

Table - Dynamic range and linearity of Shack-Hartmann quad-cells (this is same as Table 5.3, Pg. 149 of Hardy). NGAO PnS LGS WFS’s use a 4x4 pixel sub-aperture with p=1; while we choose a p of 0.5 for the fixed LGSWFS’s.

Figure apparent spot size measurement at the detector due to various effects for the fixed tomographic LGS WFS spots (left) and that of deployable PnS (TT sharpening) LGS WFS spots (right). Charge diffusion term is set to 0 to come up with a estimate of the detector platescale.

### Downlink TT mirror choice

To determine the TT mirror of choice, we need to specify the resolution and the throw required for the mirror given the bandwidth requirement from the requirements database.

Pupil de-magnification at the TT mirror= 10.949 m /(12.5 mm /1000 mm/m) = 875.92

TT resolution on sky = 1 milliarcsec (say)

[The RMS 1D tilt error is 95 milliarcsec (c.f. EBS Version 1.48)]

Hence, TT mirror resolution = 0.001 (arcsec) \* 875.92 = 0.875 arcsec = 4.2 microradians

Capture need, say is, 0.5 arcsec (on sky angle) = 0.5\*875.92 “ /206265 (“/rad) = 2.12 millirad

Based on the resolution and the capture range we choose the following mirror from Physik Instrumente’s catalog: <http://www.physikinstrumente.com/en/products/prspecs.php?sortnr=300700>

S-330.8SL has 10 mrad of tilt travel with 0.5 microrad (0.12 milliarcsec resolution on sky) open-loop resolution is the mirror of choice. The mirror has a resonance frequency of 1 KHz with a 1” diameter optic with ¼” thickness.

### The effect of using a single global focusing stage with no individual stages for the 7 LGSWFS channels:

Individual LGS WFS channels see differential focus due to two effects; viz. change in ROC of the LGS focal plane with change in distance to the sodium layer (c.f. ) and due to the finite size of the LGS asterism on sky. The physical distance between the innermost and outermost laser beacons on-sky vary with zenith angle as shown in ; this effect is quantified in . Both effects, though not negligible, are entirely deterministic given the position and geometry of the LGS asterism and so the defocus can be calibrated away by the RTC. So the preferred design choice is to use a single focusing stage for the entire LGSWFS assembly.

|  |  |  |  |
| --- | --- | --- | --- |
| Sodium layer altitude | ROC of focal plane (from Zemax) | Focal plane size | Sagitta |
| 90 km | 883.2 mm | 7.27 mm | 0.0299 mm |
| 180 km | 2064 mm | 7.27 mm | 0.0128 mm |
|  |  |  |  |
|  |  | **difference in sag =** | **0.0171 mm** |

Table - Radii of curvature of the LGS focal plane as delivered by the NGAO optical relay at 90 and 180 km Na layer object distance and the change in focus due to the changing RoC.



Figure - Schematic showing defocus between the innermost and outermost LGS due variation in physical distance of those with zenith angle.

α = 1.221 degrees (at 70 degrees off zenith pointing)

β = 7.2722 \* 10^(-2%) deg.

b = **h/cos(**α**) \*** β

x = **b\*tan(**α**)**

Where, α is the telescope DEC angle WRT zenith.

β is the angle subtended by the beacons onto the laser launch telescope

h is the Na layer altitude at zenith (90 km)

b is the physical distance between the innermost and outermost beacon at the Na layer.

X is the object distance shift between the innermost and outermost laser beacon.

|  |  |  |
| --- | --- | --- |
| Guide star radius | defocus error due to geometry of the asterism (um) | Error in waves |
| 10 | 17 | 0.0778 waves |
| 50 | 68 | 0.311 waves |

Table - shows the error due to change in focus between the innermost and outermost LGS with zenith angle. For reference λ/4 depth of focus is 147 nm of WFE and 219 um of defocus (as given by 2\*λ\*F/#2).

### LGS WFS relay performance specification

Internal WFS aberration allocation is 0.25” (FWHM). The LGS spots delivered by the OSM are 3 and 8 times smaller in (RMS) radii than the input spots from the AO relay for the fixed and deployable LGSWFS’s respectively. The OSM’s contribution corresponds to an FWHM of ~0.05 arcsec. Hence, the LGSWFS relay performance needs to have: Spot size (RMS as indicated by Zemax) at the detector = Allocation (arcsec FWHM)/2.355 (FWHM/RMS) \* 21 (um/pixel)/1.49 (arcsec/pixel) = 0.25/2.355\*21/1.49 = ~**1.5 um**

### Field stop specification

The FoV of the tomographic and PnS subapertures are 5.96 and 5.64 arcsecs respectively. A square- field stop that is 3.6 arcsecs on the edge will be positioned at the WFS focus to prevent crosstalk of LGS spots at the detector.

## Optical design and performance

### Fixed LGS WFS

#### Wavefront sensor design math

Pixel size/spot size = 0.5 (as per )

From the AO system optical design, 720 um is an arcsec.

Hence, 1.41” corresponds to 42 um (2\*21 um detector pixels).

fcollimator/flenslet \* 1/m = Plate scale at the input of the sensor(um/asec)/ Detector plate scale (um/asec)

= 720/29.78 = 24.4064 (720 is the # obtained from Zemax); we choose fcollimator= 80 mm from JML’s catalog.

We choose a commercial collimator instead of a commercial lenslet as the Fresnel Number (FN) of the lenslet is fixed and any (non-custom) commercial lenslet needs to have the exact same FN to be used in NGAO. The limited lenslet database didn’t have any match for the required lenslet FN.

d each lenslet = fcollimator/f# \* 1/(# of sub-aps) = 80/13.56 \* (1/63) = 93.6 um (choose a 80 mm focal length lens).

m = 0.084/0.0936 = 0.896

f2 = fcollimator/m \* (29.78/720) = 80/0.89699 \* (1/24.17145) = 3.68 mm (f/# lenslet = 39.42)

lenslet array Fresnel # = (d each lenslet /2)2/(f\*λ) = 1.01.

The FN term is an invariant and can be expressed as 1/(4\* λ) \* (Dtelescope/# of subaps) \* (spot sep. in radians)

The simplest possible tomographic LGSWFS with the least # of surfaces can be made with a best form singlet and a lenslet array directly imaging spots onto a detector without using a reimaging relay[[2]](#endnote-2). Such a design will have a lenslet pitch of 84 um and lenslet focal length of 2.97 mm with a 71.76 mm EFL collimator. The whole wave front sensor is compact and has only 4 surfaces with either the collimator or the lenslet serving as the detector window. Such a WFS was designed using a custom collimator and a custom lenslet. The design is available at <http://www.oir.caltech.edu/twiki_oir/pub/Keck/NGAO/WFS/fixed_lgs_wfs_norelay.ZMX>. The problem with the sensor is the complexity of alignment and procurement with no margin of error due to lack of degrees of freedom to adjust the lenslet spots onto the detector.

#### Fixed LGSWFS pick off design and performance

To accommodate mechanical packaging and keep the optical surfaces to a minimum, a 1:1 relay was chosen with a total length of 640 mm (Alex to add packaging constraints). and show the optical layout of the relay and spot diagrams they deliver. The relay has a FoV of 5” and is designed to be telecentric in order to not introduce any spurious tilts in the beam due to the incidence position of the LGS light on the pickoff. The spots sizes are 16 um RMS compared to 40 um RMS spots that the AO relay generated from the AO relay. The design for the pick off is available at <http://www.oir.caltech.edu/twiki_oir/pub/Keck/NGAO/WFS/fixed_LGS_pick_off.ZMX>



Figure - Telecentric 1:1 fixed LGSWFS pick off relay. The total length of the relay is 640 mm (limited by packaging constraints).

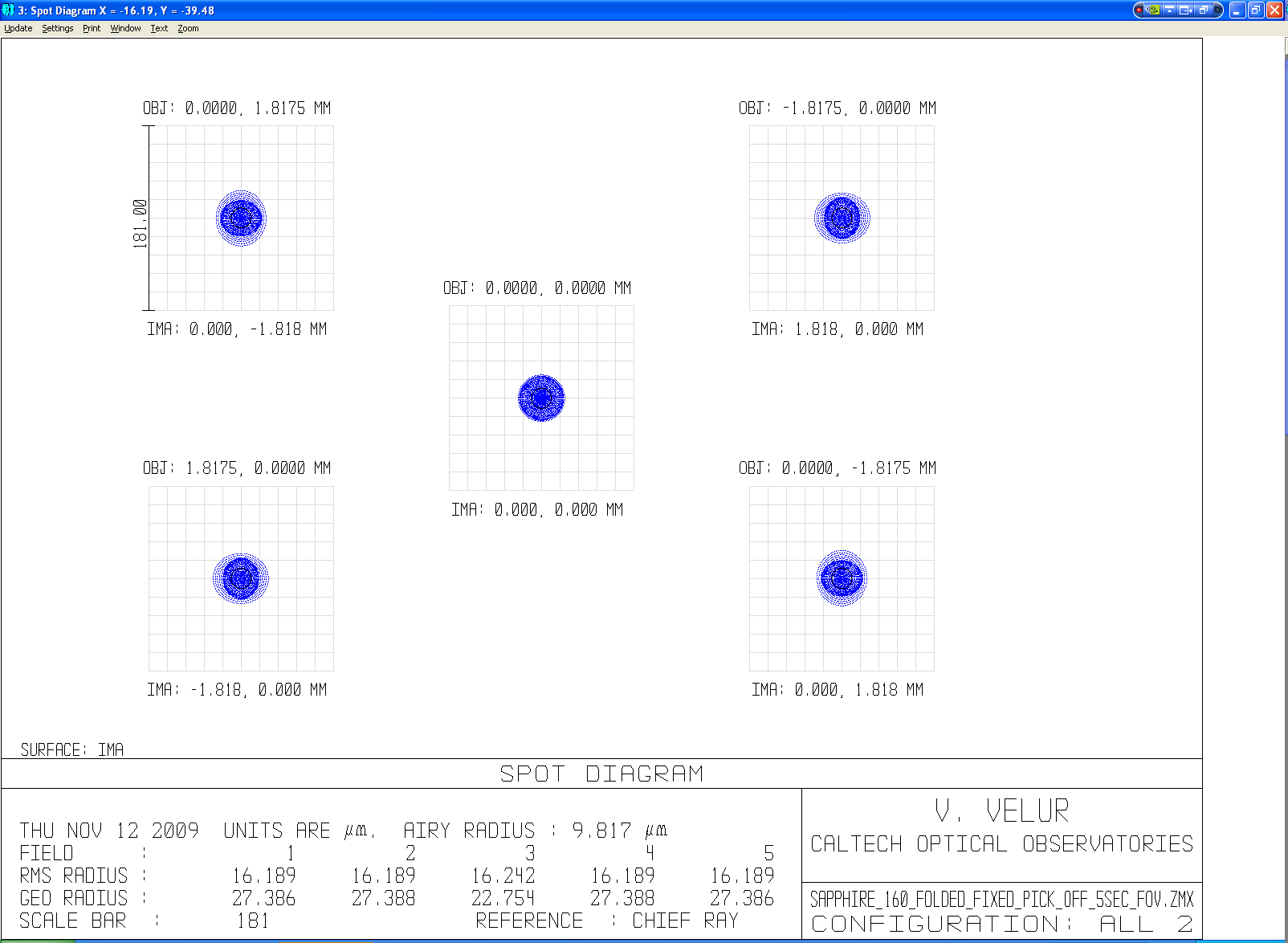


Figure - Spot diagram showing the performance of the fixed LGSWFS pick-off over a 5 arcsec FoV (scale bar corresponds to ¼ arcsec.).

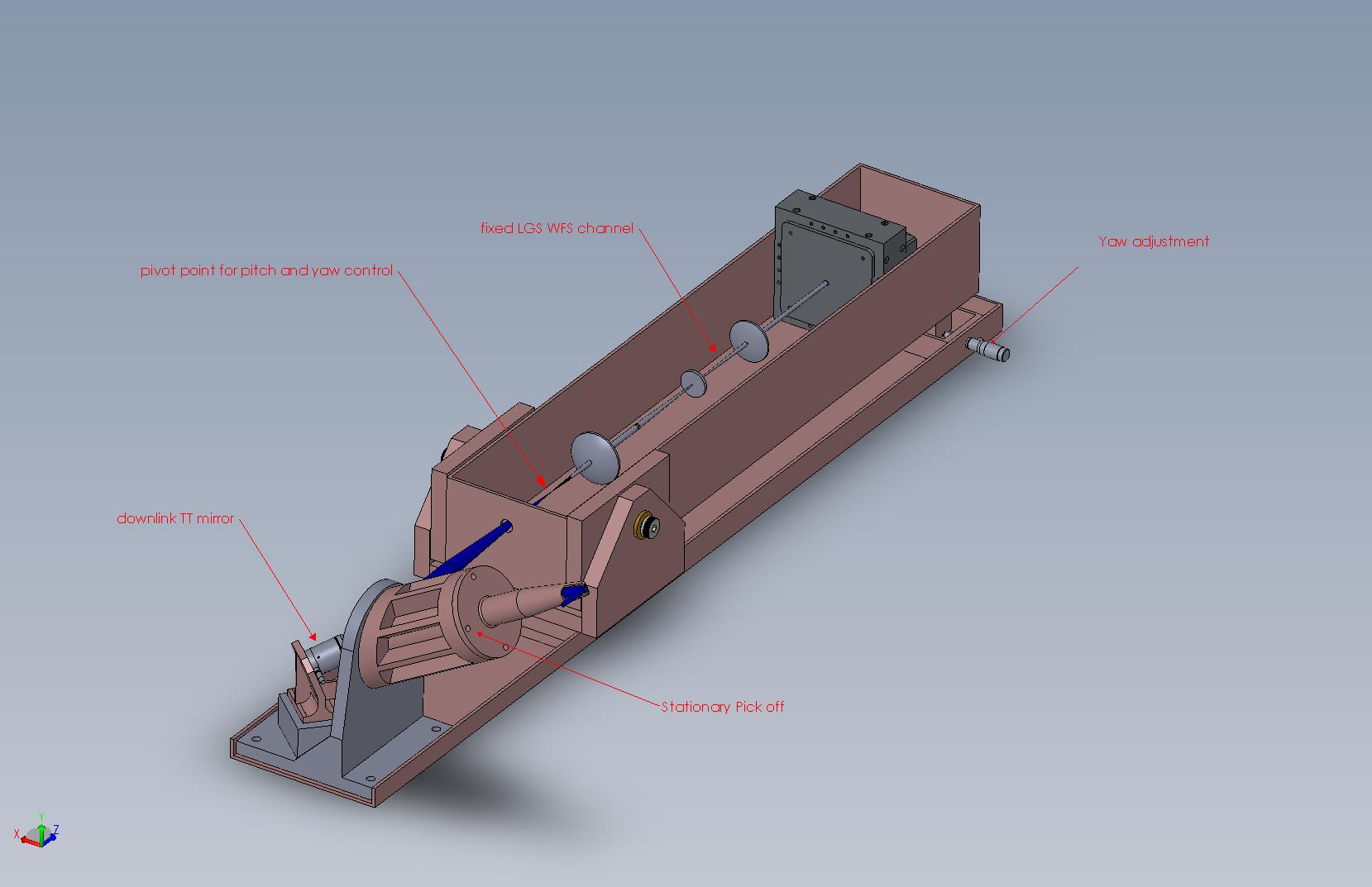


Figure - Mechanical design of stationary fixed LGSWFS channel with stationary 1:1pick-off relay with the downlink tip-tilt mirror at the relay’s pupil location. Each tomo. LGSWFS is equipped with yaw and pitch motion, which along with the downlink TT mirror can be used to align each channel to the incoming beam and keep the lenslet to LODM registration.

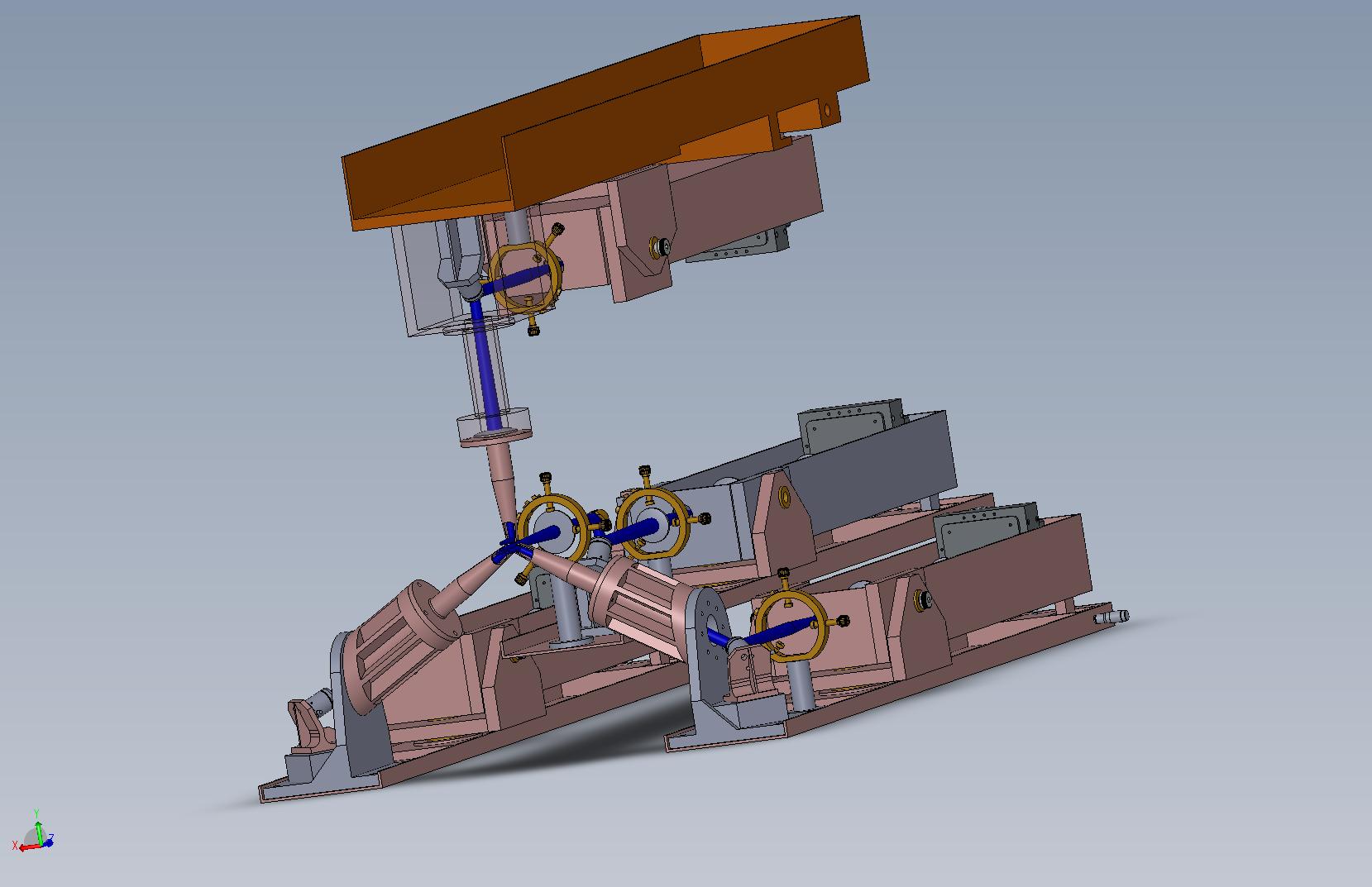


Figure – Mechanical assembly of the fixed asterism pick offs and sensors assembly showing the 4 fixed LGSWFS’s with one located in the middle and other three located equidistant from each other on a 10 arcsec circle about the central axis.

#### Fixed LGSWFS post-lenslet relay design and performance

To ensure that the requirement on the wavefront quality delivered by the WFS relay, the relay was modeled separately and the image quality of the relay assessed independently. The layout of the relay is shown in . The relay delivers sub 1um RMS spots with a 0.03% grid distortion at a de-magnification of 0.89.

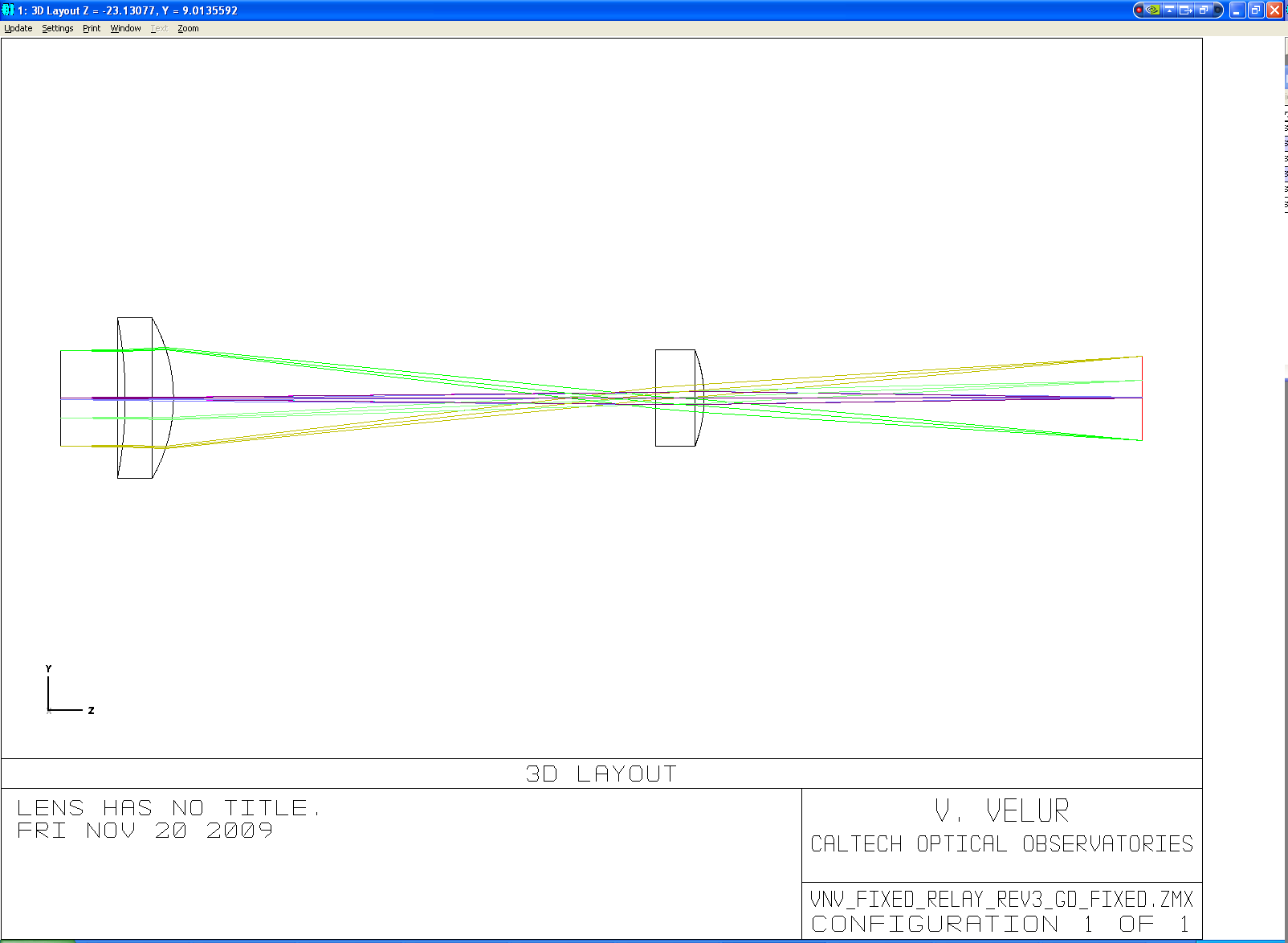


Figure - fixed LGSWFS post-lenslet WFS relay layout.

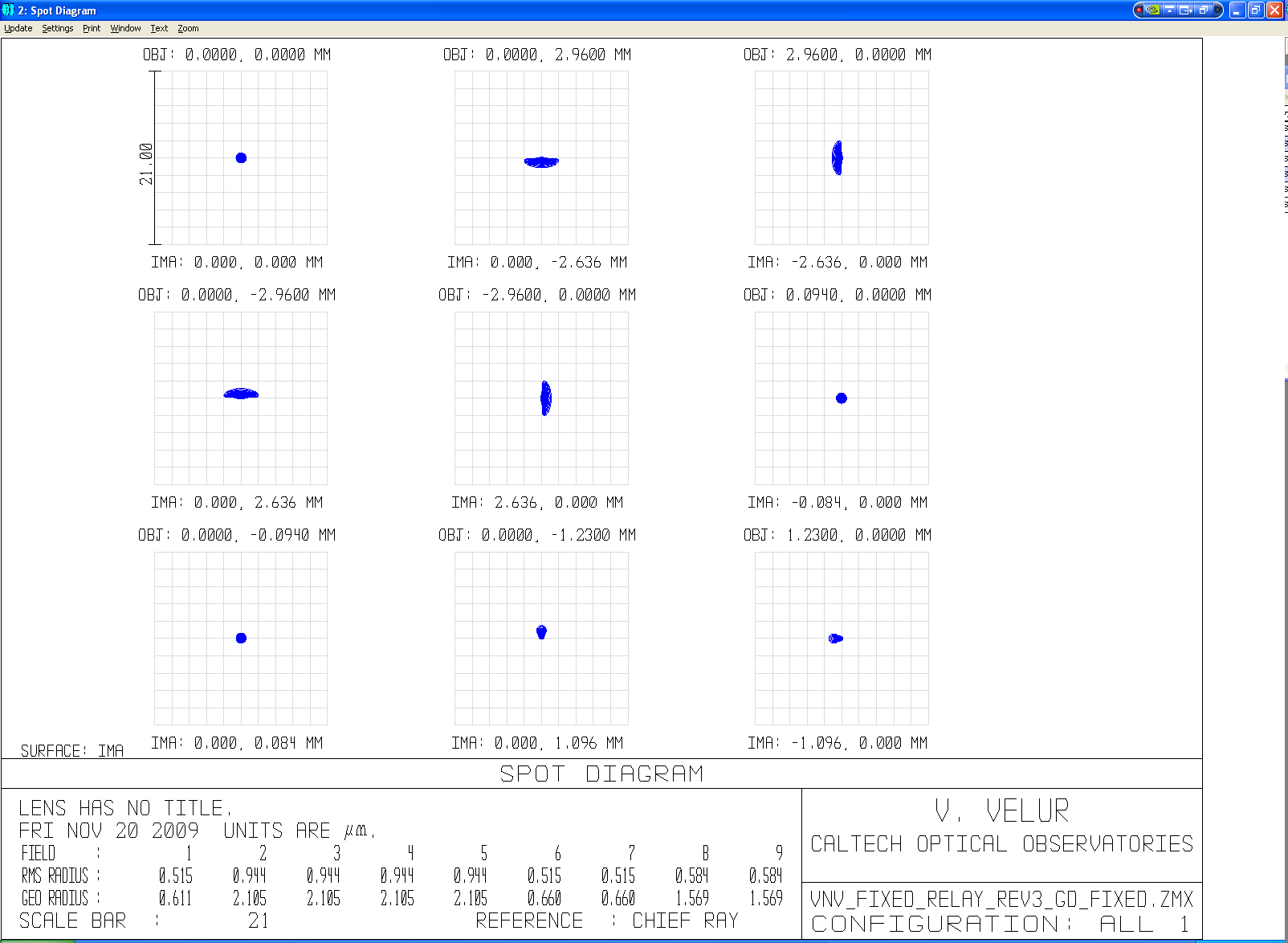


Figure – Spot diagram showing an on-axis point and 4 extreme points of the lenslet spots with the worst case spot size being 0.95 um RMS radius. Detector pixel size is 21 um for reference. Field points 6 and 7 are one lenslet spot away indicating that the magnification is matched to 84 um spot separations at the detector. The grid distortion of the relay is 0.03%.

#### Fixed WFS design and performance

The fixed LGSWFS channels use a stock collimator, a custom lenslet and a set of 2 custom relay lenses. All optical components are singlets, giving rise to a total of 10 surfaces that need to be laser line coated at 589 nm. The transmission of this module is (99.6%)10 \* 92.5% (lenslet scatter losses) = 88.86%. The transmission of the system with the pick off (2 folds + 2 lenses) is (99.6%)16 \* 92.5% = 86.75%. The layout and the spot diagram from the WFS channel are shown in and . The footprint diagram shown in indicates that the plate scale is accurate.

#### 

Figure - layout of fixed LGSWFS, The total length of the sensor is 230 mm. The relay is composed of a best-form lens for a collimator, a custom lenslet array and a set of custom singlet relay lenses.

#### 

Figure – fixed LGSWFS spot diagram showing 64x64 sub-apertures

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Figure - footprint diagram with 2 field points, on on-axis point and one 1.41 arcsec (1205.7 um) away showing that the plate scale at the detector is 0 .705arcsec/pixel

### Point and Shoot LGS WFS

#### Wavefront sensor design math

Pixel size/spot size =1.0 (as per )

Hence, 1.49” on sky corresponds to 21 um (detector has 21 um pixels).

fcollimator/flenslet \* 1/m = Plate scale at the input of the sensor(um/asec)/ Detector plate scale (um/asec)

= 720\*2/14.0939 = 102.171 (720 is the # obtained from Zemax).

d each lenslet = fcollimator/f# \* 1/(# of sub-aps)=95/27.12 \* (1/31) = 112 um

m = 0.084/0.112998 = 0.74, we choose fcollimator = 95 mm EFL from JML Optical’s catalog.

f2 = fcollimator/m \* (29.78/720) = 95/0.74337 \*(1/102.1714) = 1.25 mm (lenslet f# = 11.06)

lenslet array Fresnel # = (d each lenslet /2)2/(f\*λ) = 4.33.

Similar to the fixed LGS sensors, there exists a simple PnS LGSWFS with the least # of surfaces. The WFS will have a lenslet pitch of 84 um and lenslet focal length of 0.69 mm with a 70.62 mm EFL collimator. The whole wavefront sensor is compact and has only 4 surfaces with either the collimator or the lenslet serving as the detector window. The sensor was designed and the design is available at: <http://www.oir.caltech.edu/twiki_oir/pub/Keck/NGAO/WFS/PnS_lgs_wfs_norelay.ZMX>.

#### PnS LGS pick off design and performance

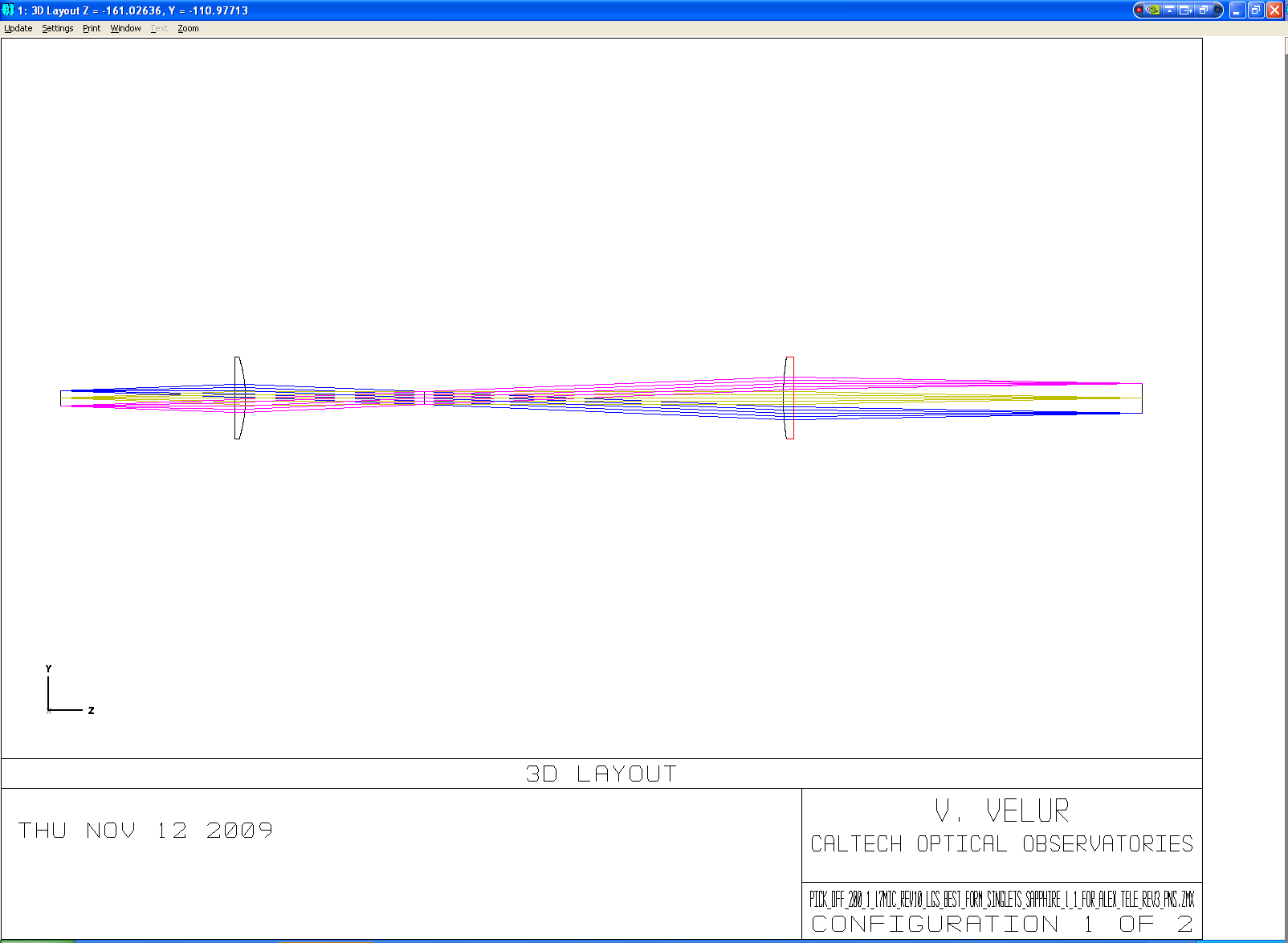


Figure – Figure showing the telecentric unfolded layout of the PnS LGSWFS pick off. The relay is 1:2 due to packaging constraints.

A 1:2 telecentric relay was designed to accommodate mechanical packaging of the theta-phi pick-off and the fast TT mirror located at the relay pupil. The total length of the relay is 528 mm. , , show the spots from the relay and the mechanical assembly of the pick-off arm and the 3 channel PnS WFS assembly. The pick off mirror location is +10, -5 and -20 mm from the focal plane for the 3 PnS wavefront sensors. The light that is incident on the pick-off gets folded and collimated to form a pupil at fast TT mirror which folds the beam down to a pair of periscope mirrors. The pick-off mirror and the fast TT mirror are part of the rotatable lever and the periscope mirrors are part of a rotating crank. The combination of these two rotations facilitates positioning the pick-off anywhere in the field. There is a need to undo the combined effect of these rotations to keep the LODM pupil orientation fixed onto the lenslet array. The design of the pick-off relay can be downloaded from <http://www.oir.caltech.edu/twiki_oir/pub/Keck/NGAO/WFS/pns_pick_off.ZMX>.

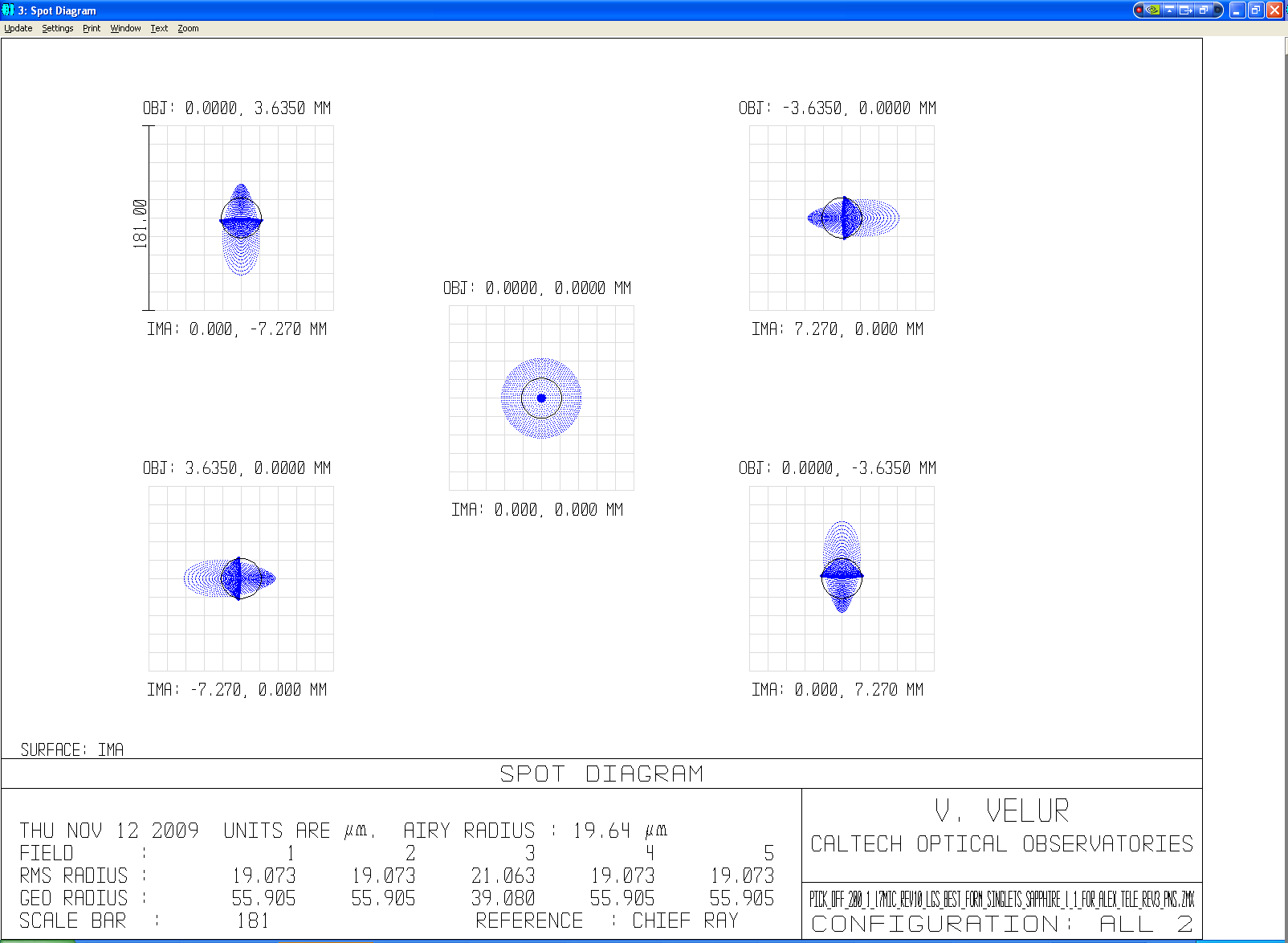


Figure – Spot diagrams from the 1:2 PnS pick off relay showing spots with rms spot radius of 21 um as compared to 130um rms spots delivered by the AO relay. For reference 101 um is 1/4 arcsec.

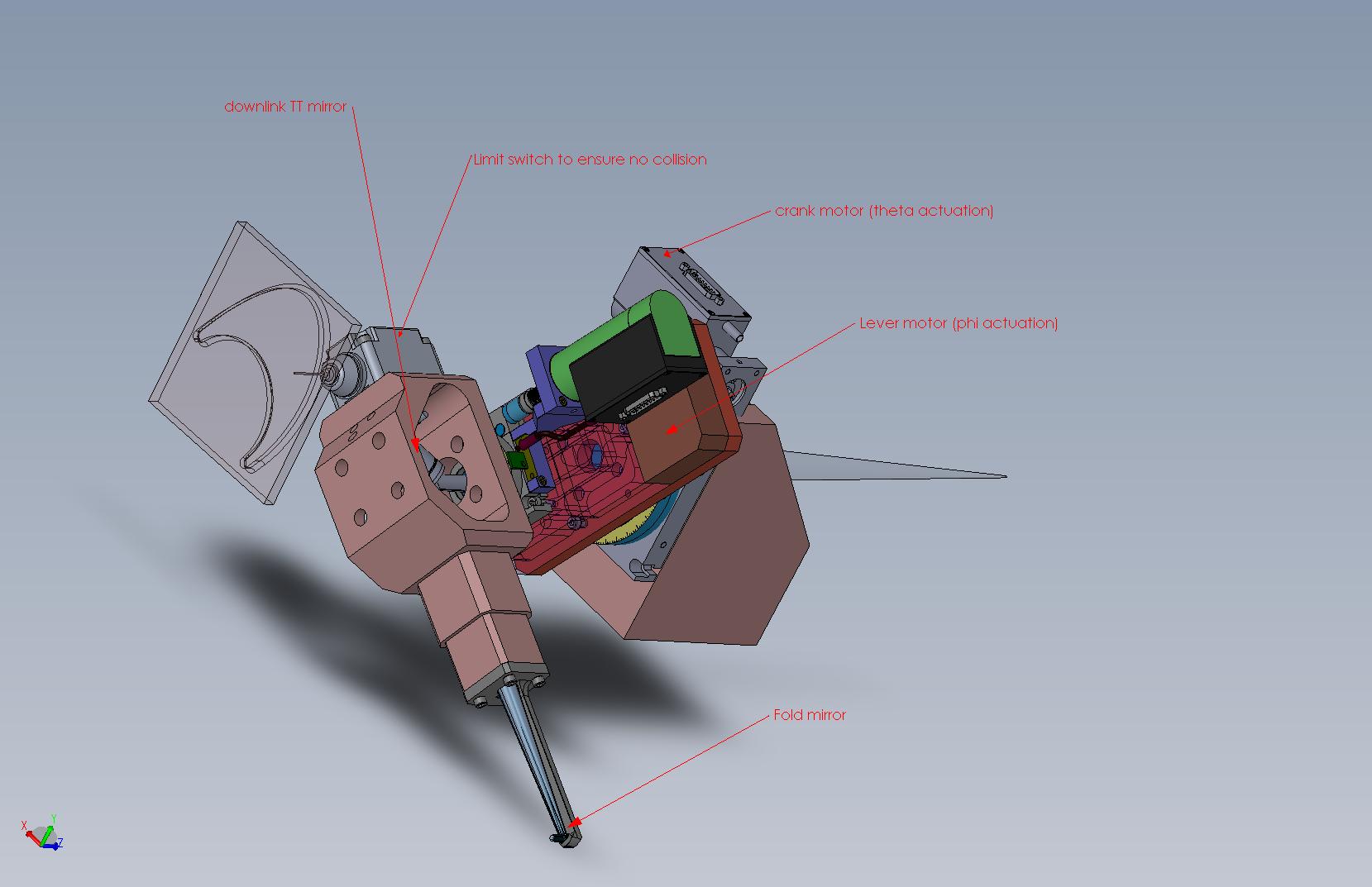


Figure - mechanical assembly of a single deployable PnS pick-off showing the theta-phi mechanism with a downlink TT mirror located at the pupil. The blue and green parts are commercial motors that move the crank and lever.

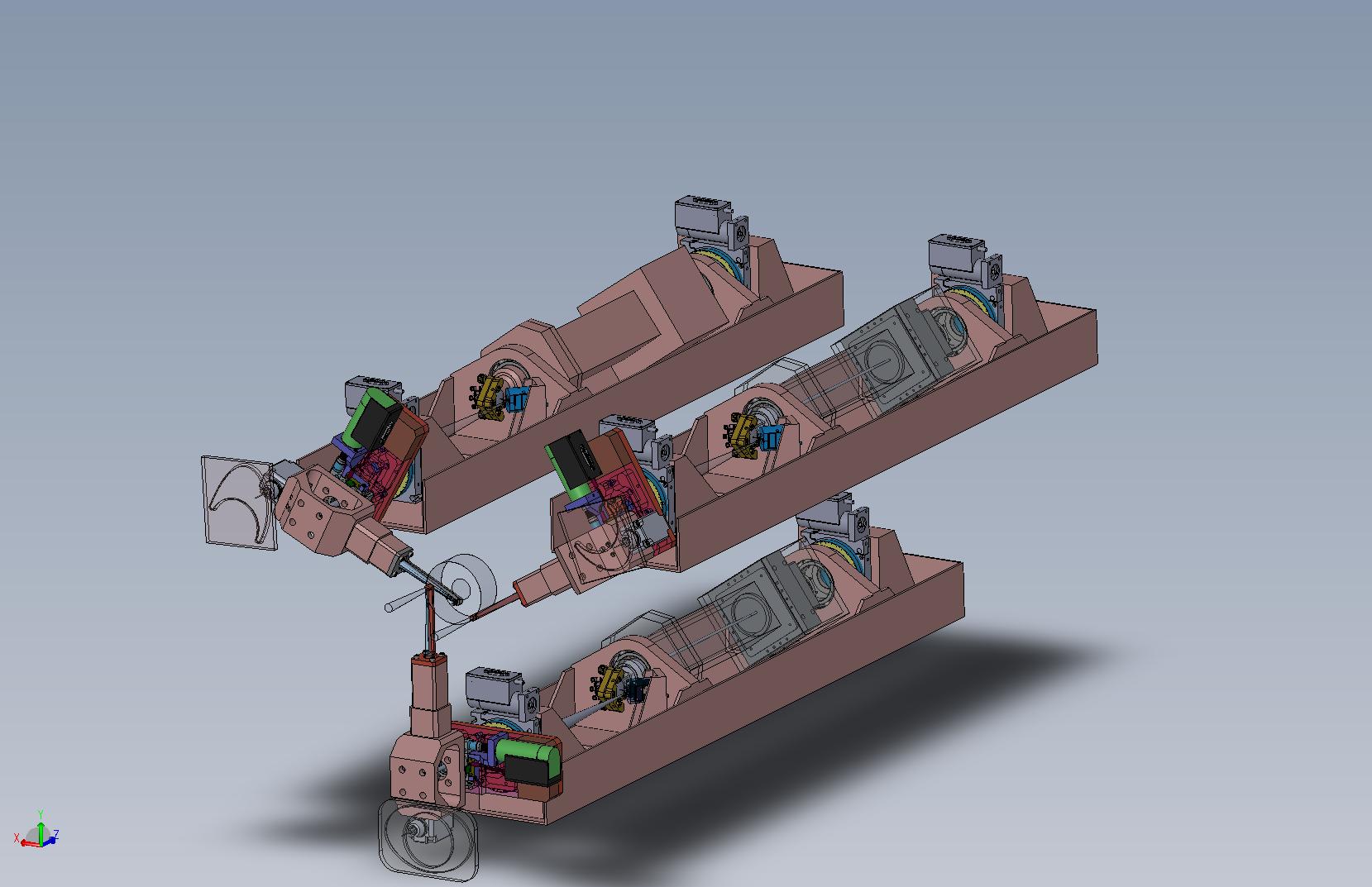


Figure – Mechanical assembly of the PnS WFS channels showing the lenslet, the post-lenslet relay and the detector mounted on a bearing and a rotary stage to keep the lenslet and the LODM actuators registered with respect to each other for any pick off position in the FoR. Each of the PnS WFS channel is also equipped with a TT mirror near the focus of the pick-off relay to keep the DM pupil registered onto the lenslet; this is necessary to eliminate pupil wander

#### PnS WFS Post-lenslet relay design and performance

The post lenslet relay was modeled separately for the PnS sensor and the performance of the relay measured. Since the lenslet spots are f/11 the design required doublets rather than just a pair of singlets. Models were built with single doublet and a singlet field lens with unsatisfactory performance. The 2 doublet relay gives sub um (RMS) spots with negligible grid distortion.

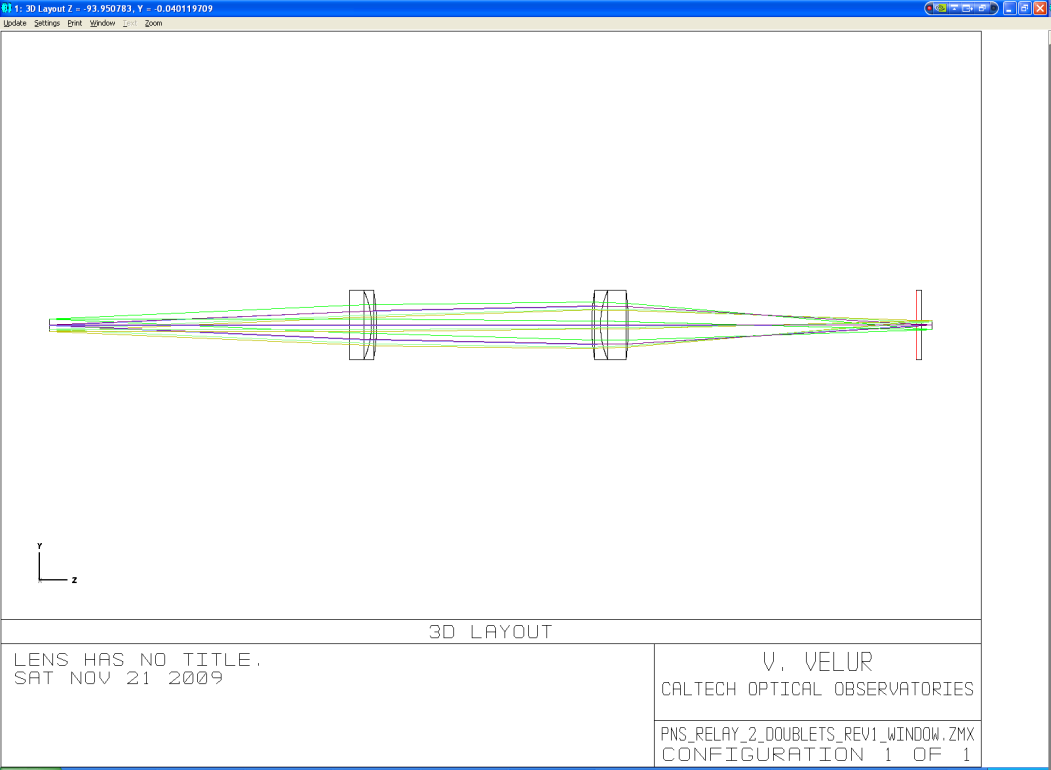


Figure – Shows the layout of the post lenslet relay in the PnS LGSWFS, the length of the relay is 300 mm.

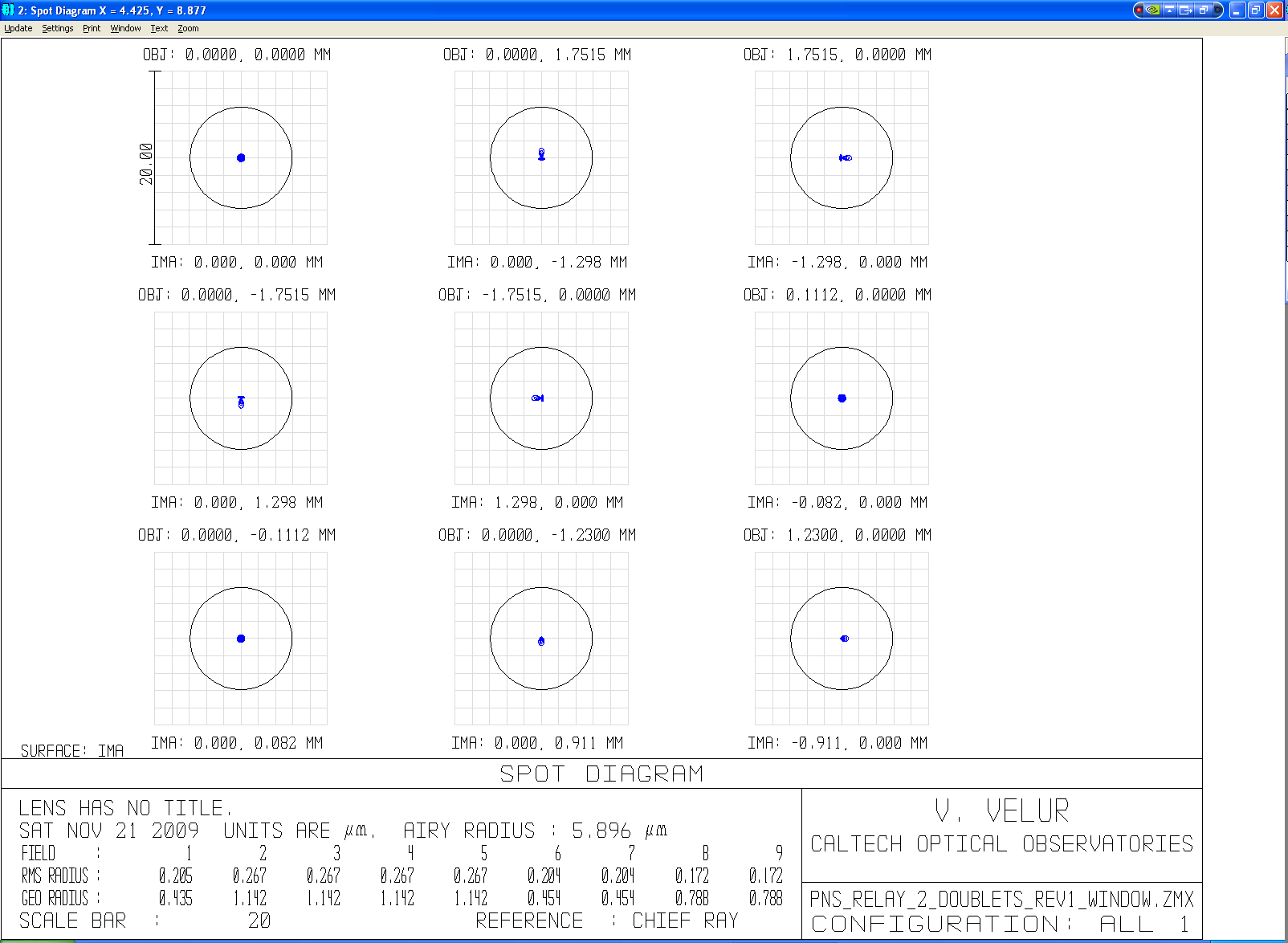


Figure - Spot diagrams of the relay with on-axis and extreme field points. There are also 2 field points to indicate that the magnification is correct and 2 more located at 1/√2 of the field size. The grid distortion of the relay is 0.001%.

#### WFS design and performance

The PnS WFS also uses a commercial best-form lens followed by a custom lenslet and relay lenses. The design of the WFS can be downloaded from: <http://www.oir.caltech.edu/twiki_oir/pub/Keck/NGAO/WFS/PnS_lgs_wfs_doublets_rev1_window.ZMX>. The WFS spots are shown in Figure 27 and a footprint diagram was used to verify the plate scale of the sensor. The total length of the sensor is 490 mm.

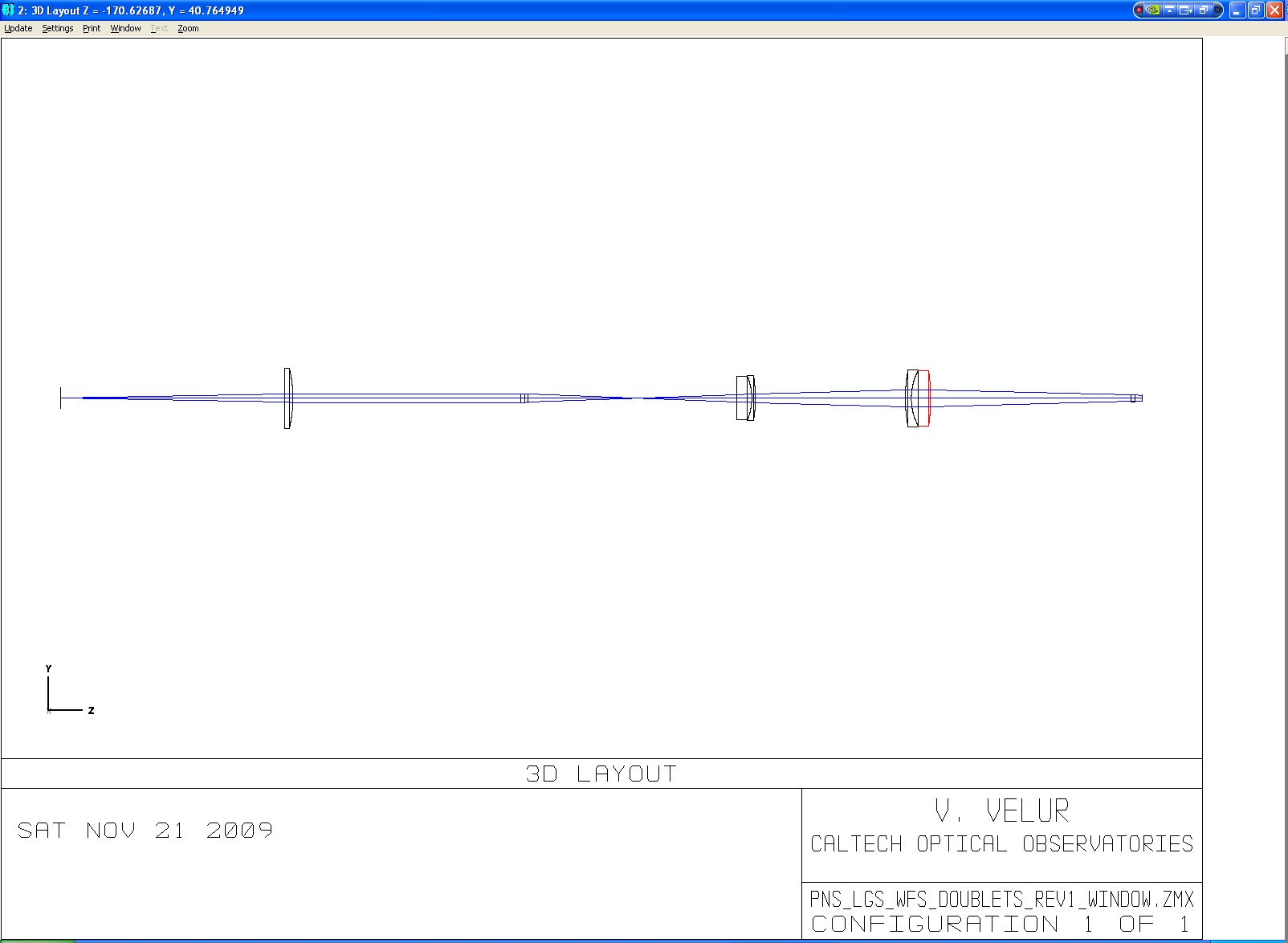


Figure - layout of the PnS WFS; the total length of the sensor is 490 mm. (I can make the relay longer to get better spots at the detector).

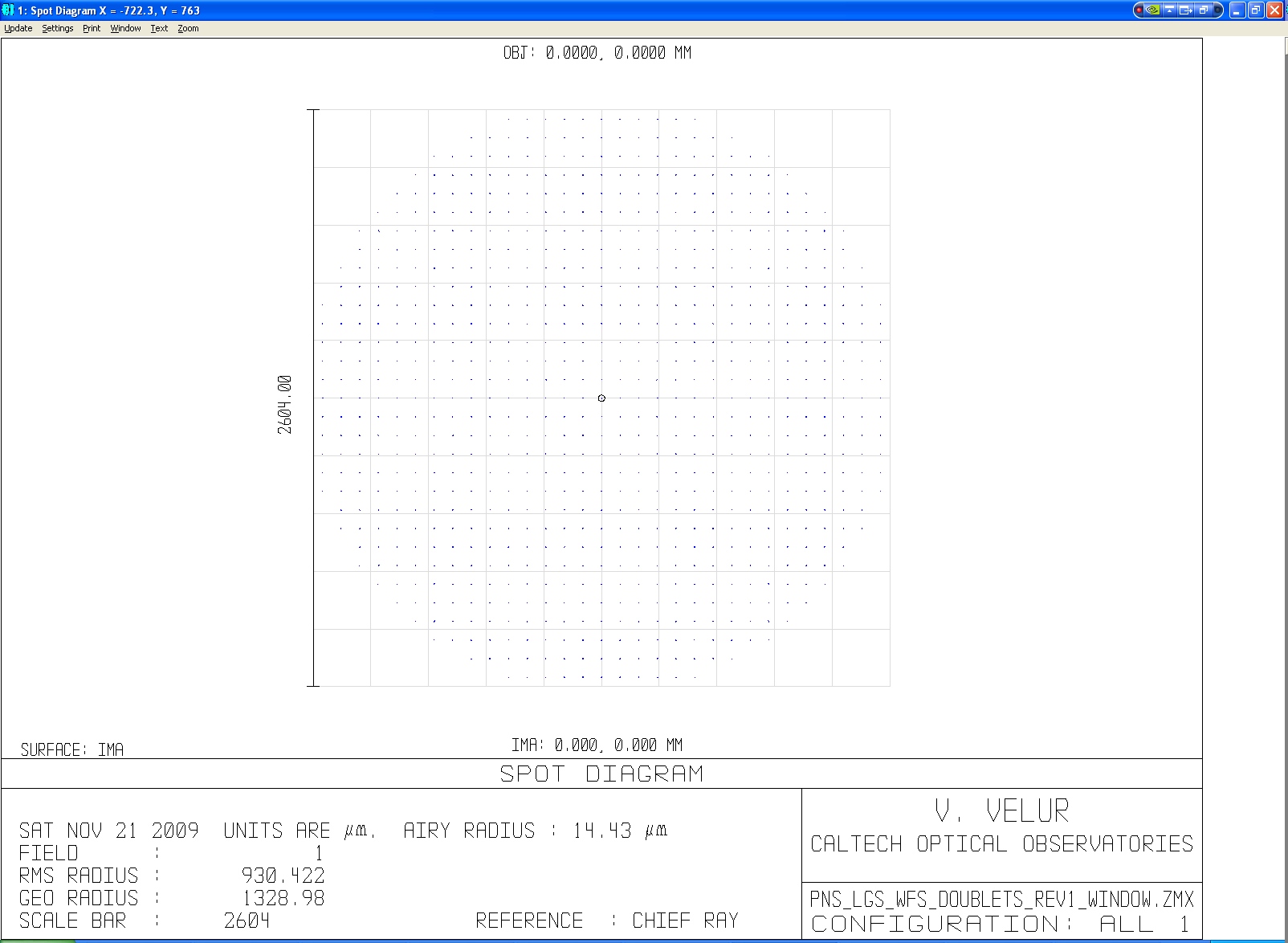


Figure - spot diagram at the detector

### Performance of the sensors with the AO relay

## Mechanical Design

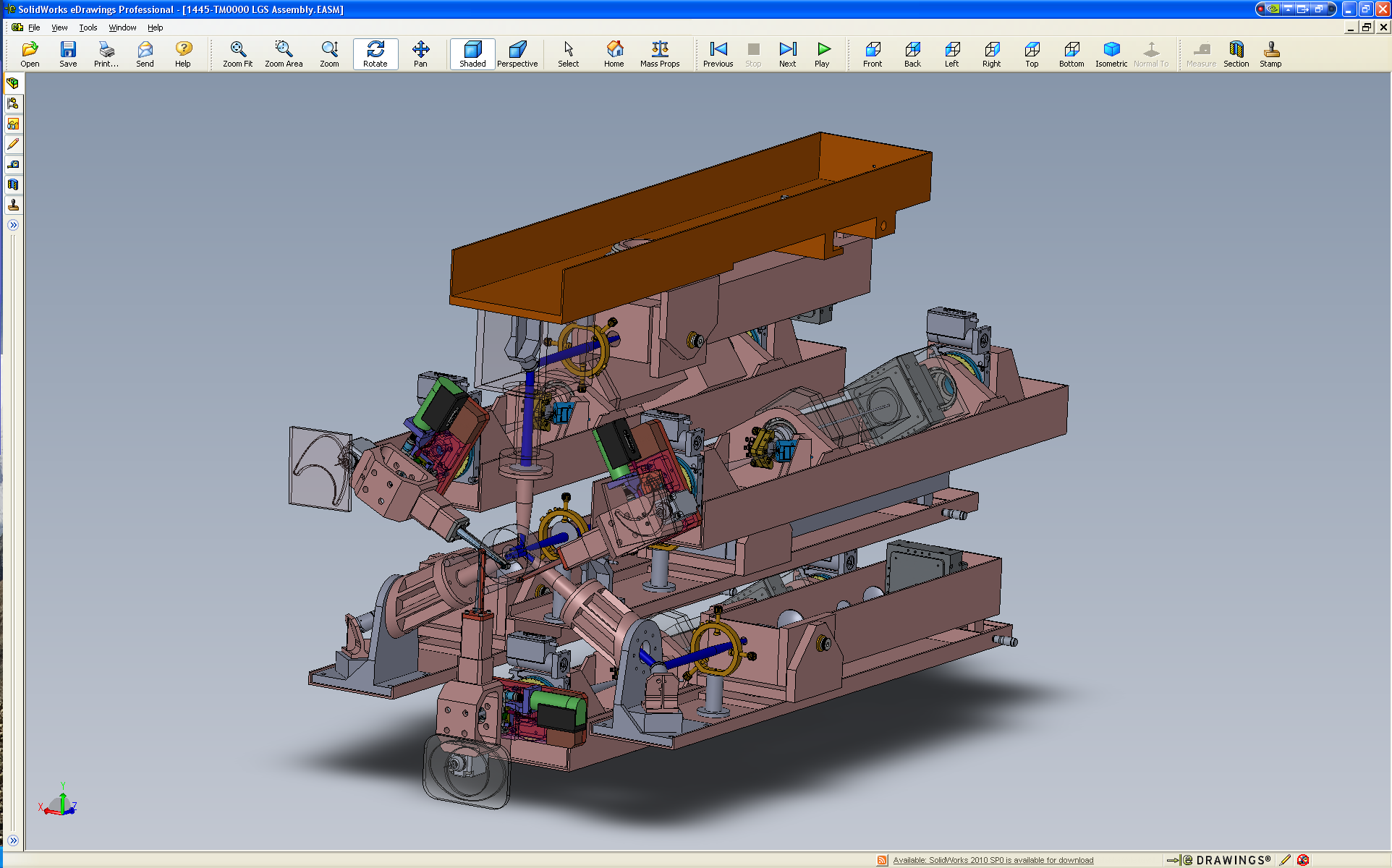


Figure - mechanical assembly of the LGSWFS

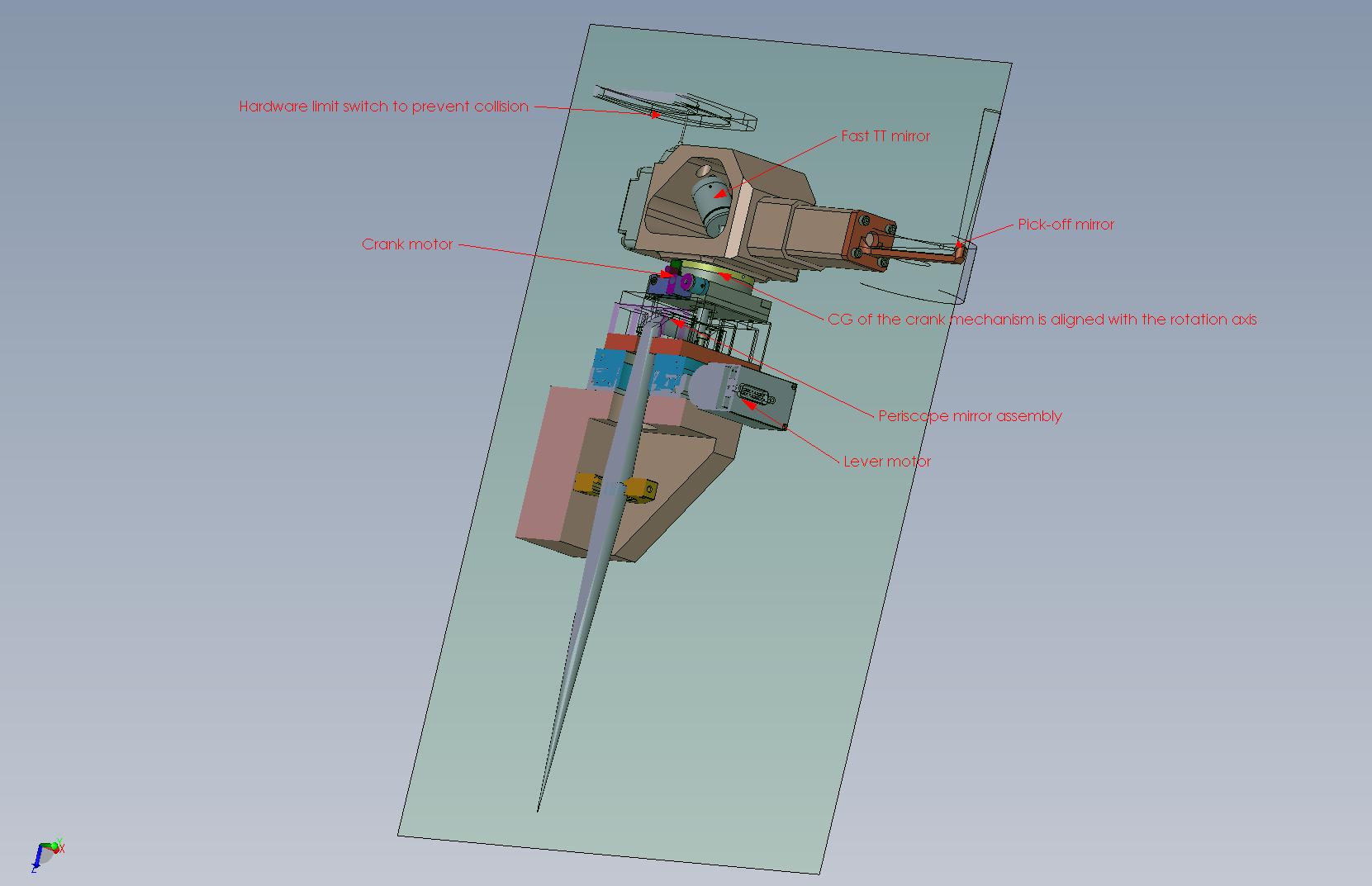


Figure - part cross sectional view of the PnS pick-off

### PnS and tomo. WFS pick-off and WFS relay

shows a partial cross-sectional view of the PnS pick off. The crank lever is designed so that its center of gravity is aligned to the axis of rotation and hence there is no unbalanced torque at any position of the crank arm. Similarly a counterweight on the lever ensures that the lever motor sees very minimal torque during on-sky observation. A Honeywell 8SL125 micro-switch and a custom contour milled tracker serve the purpose of a hardware limit switch so as to prevent collision of the pick-off arms. The crank and lever motors use PI’s M037 and M-038 drives. M-037 rotation stages are equipped with ultra-precise worm gear drives allowing unlimited rotation in either direction. An integrated spring preload eliminates backlash. Double-row ball bearings allow zero backlash, high load capacity and extremely low wobble. Model M-037.DG is closed-loop DC motors with shaft-mounted position encoders and precision gearheads providing 3.5 μrad at a design resolution of 0.6 μrad. Model M-038.DG1 is equipped with a closed-loop DC motor with shaft-mounted position encoder and precision gearhead providing minimum incremental motion of 3.5 μrad at a design resolution of 0.6 μrad[[3]](#endnote-3). A frictionless high-precision flexure based PI’s *S-330.8SL* TT stage with an invar platform houses the TT mirror. This stage has excellent temperature stability and works all the way to -20 degrees C. Calculations in Section 5.1.2 show that this mirror amply serves the purpose. The specifications for the TT mirror can be found at: <http://www.physikinstrumente.com/en/products/prspecs.php?sortnr=702900>. There is a pair of periscope mirrors mounted on the lever motor which swivel. There is a focusing lens past the second periscope fold mirror. Appropriate jigs will be designed to mount the mirrors at the exact angle onto each surface on which it is to be held.

The fixed asterism uses a simpler stationary pick-off. A snout-like part will hold the pick-off mirror that folds the light into a barrel with a collimator followed by a TT mirror (also a PI *S-330.8SL*). The specs for the TT mirror can be found at <http://www.physikinstrumente.com/en/products/prspecs.php?sortnr=300700>. There is a focusing lens following the TT mirror that feed light to the WFS optics.

U-channels are used to house all 7 WFS optics and detector to keep the deflection to below 1/10th of the finest sub-aperture. The PnS sensors have the lenslet-to-detector part of the relay mounted on bearings at either end to facilitate rotation by just overcoming only sliding friction. There is a need to rotate about 40 (TBC) degrees and hence the camera cables will be conveyed via appropriate cable routing system. This cable management system is still to be designed.

### Baffles, Enclosure and linear stage

Each WFS will be baffled to reduce effects of Rayleigh backscatter effects that will enclose the whole relay except for the 3.6 arcsec field-stop. A enclosure made of sheet metal over the aluminum structure will be used to keep the LGSWFS clean. The whole WFS assembly shall be mounted on a 205 mm travel linear stage. An Aerotech ABL20030 stage with 300 mm travel will be used to move the whole assembly to track the change in distance to the Na-layer. The specs for the stage can be found at <http://www.aerotech.com/products/airbearing/abl2000specs.html>. The stage is a fully-preloaded air-bearing stage with a brushless linear motor. The package is zero-maintenance.

### Pupil registration and TT corrector

Because the LGS light path to the WFS is not perfectly telecentric it is necessary to register the DM actuators and the lenslet for each point in the field for the PnS WFS (if the effect is not measured and calibrated). For this process we have a slow TT mirror near the pick-off focus to register the LODM actuators to the lenslet. We also provide a pitch and yaw mechanism to align the fixed LGS WFS lenslets to the LODM. Each LGS arm has a downlink TT mirror to correct the differential motion of LGS light WRT the science light at the pupil formed in the pick-off mechanism.

## Requirements compliance

## Risk and risk mitigation plan

## Work left to do

* 1. Stray light (including Rayleigh scatter) analysis
  2. Simplification of the Optical Design of sensors if possible.
  3. Try to redesign the plano-(parabolic) convex lens to try and provide less aberrated LGS spots at the LGS assembly input.
  4. Cost reduction by finding more economical components for motion control.
  5. Draft interface documents between the LGSWFS assembly and the various other sub-systems.

1. [KAON 644 - Build-to-Cost Architecture Wavefront Error Performance](http://www.oir.caltech.edu/twiki_oir/bin/viewfile/Keck/NGAO/NewKAONs?rev=3;filename=NGAO_B2C_architecture_performance_v4.pdf) [↑](#endnote-ref-1)
2. [Construction and testing of the wavefront sensor camera for the new MMT adaptive optics system, P. C. McGuire et. al.](http://caao.as.arizona.edu/publications/wfs6.pdf) [↑](#endnote-ref-2)
3. <http://www.physikinstrumente.com/> [↑](#endnote-ref-3)