



NGAO Wavefront Error Budget Keck Adaptive Optics Note 471

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1 Wavefront Error Budget Spreadsheet

This study was conducted using a Microsoft Excel spreadsheet developed over several years as an engineering tool for evaluation of adaptive optics system performance. The primary purpose of the spreadsheet is to compute adaptive optics and instrumental wavefront error budgets for different architectures and science cases, along with Strehl ratios computed using the Marechal approximation. The spreadsheet also computes ensquared energy fractions using a core/halo model for the point spread function, and calculates sky coverage estimates for tip tilt guide stars employed in laser guide star architectures from common star density models. This study used version 1.18 of the spreadsheet.

The spreadsheet functionality is embedded in a series of 35 individual Excel sheets, listed in Table 1. Roughly speaking, each sheet effects calculations related to a particular error term, and these individual error terms are RSS'd together to provide an estimate of the adaptive optics error budget. The Excel solver may be used to perform a conjugate gradient search that finds the system parameters which optimize the value of another parameter. Examples of parameters that may be varied include the high order wavefront sensor frame rate, the laser asterism radius, and the brightness and angular offset of the tip tilt guide star. In this study, the Excel solver was used to maximize the H band Strehl ratio.

Sheet Name	Description
Input Summary	Selection of science case and system architecture
Optim	Wavefront error budget table, used to run optimizer
EE	Ensquared energy estimates from core/halo PSF model
Tel	Uncorrectable static and dynamic telescope aberrations
Atm	Vertical turbulence and wind profiles
HO Flux	NGS photodetections in high order wavefront sensor
LGS Flux	LGS photodetections in high order wavefront sensor
HO Cent	Centroid error in high order wavefront sensor
HO Meas	Measurement error in high order wavefront sensor
FA Tomog	Error arising from tomographic reconstruction from multiple guide stars
Ast Def	Deformation of LGS asterism due to uplink beam wander
Na H	Error arising from altitude changes of the sodium layer
Fit	High order fitting error
Alias	High order aliasing error
Stroke	Tip tilt and deformable mirror stroke requirements
Hyst	Error arising from deformable mirror hysteresis
Go_to	Go-to control error for MEMS mirrors
Dig	Actuator digitization error
TT Flux	NGS photodetections in tip tilt sensor
TT Meas	Measurement error in tip tilt sensor
Bandw	High order and tilt servo errors, error arising from telescope pointing jitter
Scint	Errors arising from scintillation in the high order wavefront sensor
Aniso	Errors arising from anisoplanatism
CA	Centroid anisoplanatism error
Chromatic	Errors arising from chromatic dispersion
Atm Dispersion	Atmospheric dispersion calculations
Cal	Calibration errors
Notes	Notes
Sky Coverage	Calculation of sky coverage
Spagna	Near infrared star density model from NGST study
Bachall	Visible star density model
Parenti	Near infrared star density model from the Infrared Handbook
Allen	Visible star density model from Allen's Astrophysical Quantities
Specific Fields	Notes on specific science cases

Table 1: Individual pages in the Excel spreadsheet. The first page is used for selection of the science case and AO architecture, and the second is used for running the optimizer, and presents a summary of the wavefront error budget. The remaining pages effect calculations of the various error budget terms using models of the underlying error processes. In this spreadsheet, errors are assumed independent, and are added in quadrature to arrive at an overall error budget.

Science Case	AO Architecture
Io	NGSAO
Kuiper Belt Objects	LTAO
Exo Jupiter	LTAO
Extended Groth Strip	MOAO
Galactic Center	LTAO

Table 2: NGAO science cases and adaptive optics architectures. The three architectures under consideration are natural guide star AO (NGS), laser tomography AO (LTAO) and multiobject AO (MOAO).

Layer Height (m)	Layer Strength (m ^{1/3})	Wind Speed (m/s)
0	5.85e-13	6.4
2100	1.12e-13	10.5
4100	1.41e-14	15.6
6500	3.13e-14	18.4
9000	5.18e-14	14.6
12000	5.09e-14	7.5
14800	3.20e-14	4.5

Table 3: Turbulence and wind profiles assumed in these error budgets. The integrated turbulence profile has a value of 2.61e-13 m^{1/3}, with $r_0 = 18$ cm, a $\theta_0 = 1.37$, $d_0=2.4$ m, and $f_G=41$ Hz.

2 Science Cases

This study presents optimal error budget solutions for five science cases selected as representative of the NGAO system. These five science cases, together with the adaptive optics architecture required to carry out the observation, are listed in Table 2. An error budget was developed for each science case that maximized the H band Strehl ratio when appropriate system parameters were allowed to vary. For each case the variable parameters are tabulated, along with any constraints placed on these parameters. (e.g. positivity constraints or physical limits on device characteristics.) The resulting optimal error budget is tabulated for each science case. These error budgets were computed assuming that the observations were to be carried out at zenith, with the baseline turbulence and wind profile listed in Table 3 (the CN N2 profiles).

Versions of the Excel spreadsheet are available for each science case at URL http://www.oir.caltech.edu/twiki_oir/bin/view.cgi/Keck/NGAO/SystemArchitecture For each science case, the spreadsheet contains the tabulated set of optimization parameters. This is intended to permit users to download and inspect the spreadsheet for each science case without the need to modify and optimize any parameters.

2.1 Io

An NGAO wavefront error budget for observations of the planet Io is shown in Figure 1. Io is used as the tip tilt and high order natural guide star for this science case. The AO frame rate was capped at 2.5 kHz and the number of high order subapertures was fixed at 64 across the pupil. In this scenario there were no optimization constraints, as shown in Table 4. The optimizer provided the solution in Figure 1 with a high order wavefront error whose largest term is uncorrectable telescope aberrations and a tip tilt error dominated by residual telescope pointing jitter. This scenario delivers an H band Strehl ratio of 73%.

Variable Parameters	High order integration time	$\geq .0004$ sec
Optimized Parameter	H band Strehl Ratio	=73%

Table 4: Optimized parameter and constraints for the Io observing scenario.

Keck Wavefront Error Budget Summary

Mode: NGAO NGS
 Instrument: TBD
 Observation: Io

		Science Band								
		u'	g'	r'	i'	Z	Y	J	H	K
λ (μm)		0.36	0.47	0.62	0.75	0.88	1.03	1.25	1.84	2.20
$\Delta\lambda$ (μm)		0.06	0.14	0.14	0.15	0.12	0.12	0.16	0.29	0.34
λ/D (mas)		7	10	13	15	18	21	26	34	46

High-order Errors (NGS Mode)	Wavefront Error (rms)	Parameter	Strehl Ratio (%)									
Atmospheric Fitting Error	41 nm	64 Subap										
Bandwidth Error	20 nm	220 Hz (-3db)										
High-order Measurement Error	25 nm	5 mV										
LGS Tomography Error	0 nm	1 natural guide star										
Astigmatism Deformation Error	0 nm	0.50 m LLLT										
Multiplex Error	20 nm	18 zenith angle, H band										
Scintillation Error	15 nm	0.38 Scint index, H-band										
WFS Scintillation Error	10 nm	Ailoc										
Uncorrectable Static Telescope Aberrations	43 nm	64 Acta										
Uncorrectable Dynamic Telescope Aberrations	8 nm	DeKans Ph.D										
Static WFS Zero-point Calibration Error	25 nm	Ailoc										
Dynamic WFS Zero-point Calibration Error	20 nm	Ailoc										
Leaky Integrator Zero-point Calibration Error	15 nm	Ailoc										
Go-to Control Errors	0 nm	Ailoc										
Residual Na Layer Focus Change	0 nm	30 m/s Na layer vel										
DM Finite Stroke Errors	1 nm	4.0 μm P-P stroke										
DM Hysteresis	13 nm	from TMT										
High-Order Aliasing Error	9 nm	64 Subap										
DM Drive Digitization	1 nm	16 bits										
Uncorrectable AO System Aberrations	30 nm	Ailoc										
Uncorrectable Instrument Aberrations	30 nm	TBD Instrument										
DM-to-lenslet Misregistration	15 nm	Ailoc										
DM-to-lenslet Pupil Scale Error	15 nm	Ailoc										
Angular Anisoplanatism Error	14 nm	0.5 arcsec										
Total High Order Wavefront Error	96 nm	97 nm	High Order Strehl	0.07	0.21	0.40	0.54	0.64	0.72	0.80	0.88	0.93

Tip/Tilt Errors	Angular Error (rms)	Equivalent WFE (rms)	Parameter	Strehl ratios (%)								
Tilt Measurement Error (one-axis)	0.05 mas	1 nm	5.0 mag (mV)									
Tilt Bandwidth Error (one-axis)	3.44 mas	96 nm	10.5 Hz									
Tilt Anisoplanatism Error (one-axis)	0.00 mas	0 nm	0.0 arcsec									
Residual Centroid Anisoplanatism	0.00 mas	0 nm	NGS α reduction									
Residual Atmospheric Dispersion	0.83 mas	15 nm	20 α reduction									
Science Instrument Mechanical Drift	0.04 mas	1 nm	Ailoc 0.25 mas / min									
Long Exposure Field Rotation Errors	0.08 mas	1 nm	Ailoc 0.5 mas / min									
Residual Telescope Pointing Jitter (one-axis)	5.03 mas	77 nm	29 Hz input disturbance									
Total Tip/Tilt Error (one-axis)	6.2 mas	97 nm	Tip/Tilt Strehl	0.19	0.29	0.42	0.51	0.60	0.67	0.75	0.84	0.90

Total Effective Wavefront Error	135 nm	Total Strehl (%)	0.01	0.06	0.17	0.28	0.38	0.48	0.60	0.73	0.84
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Sky Coverage	Galactic Lat.	30 deg
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Corresponding Sky Coverage	0.0%	This fraction of sky can be corrected to the Total Effective WFE shown
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Assumptions / Parameters									
r_0	0.175 m	at this zenith	Wind Speed	7.76 m/s	Zenith Angle	18 deg			
Theta0_eff	1.28 arcsec	at this zenith	Outer Scale	50 m	HO WFS Rate	3299 Hz	SH	using	CCID56
Sodium Abund.	4×10^8	atoms/cm ²	LGS Ast. Rad.	0.21 arcmin	HO WFS Noise	3.3 e- rms			
Science Target:	BCAO				HOWFS anti-aliasing	YES			
LOWFS Target:	NGS	Num TT: 0	Num 3x3:	0	LO WFS rate	200 Hz	NGS	using	CCID56
LOWFS Star Type:	G	Num TTFA: 0	Num HOWFS:	1	LO WFS Noise	3.3 e- rms			

Figure 1: Wavefront error budget for the Io observing scenario.

2.2 Kuiper Belt Objects

An NGAO wavefront error budget for observations of a Kuiper Belt Object is shown in Figure 2. This observational scenario uses 6 laser beacons in an LTAO configuration, with a natural guide star used for tip tilt guiding. H band Strehl ratio was optimized by allowing the parameters in Table 8 to vary under the constraints indicated in this table. The optimizer chose a solution with a high order control loop rate of nearly 2.5 kHz and with the maximum number of subapertures. The optimal LGS asterism radius was about 30 asecs.

The tip tilt guiding parameters were optimized subject to the constraint of 10% sky coverage. With this sky coverage constraint, the optimizer chose a tip tilt guide star with $m_V=19.5$ from a field of 70 asecs, and ran the tip tilt control loop at 550 Hz. These tip tilt guide star parameters are to be interpreted in a statistical sense, in that a guide star of visual magnitude ≤ 19.5 will be available in a field of size 70 asec over 10% of the sky.

In this error budget, the dominant term in the high order budget was tomography error. The dominant term in the tilt error budget is tilt anisoplanatism.

Variable Parameters	High order integration time	No Limit
	Subaperture width	$\geq .171$ m (≤ 64 subaps)
	Tip tilt guide star brightness	No Limit
	Tip tilt integration time	No Limit
	Tip tilt guide star search radius	No Limit
	LGS asterism radius	No Limit
	Sky Coverage	=10%
Optimized Parameter	H band Strehl Ratio	56%

Table 5: Optimized parameter and constraints for the Kuiper Belt Object observing scenario.

Keck Wavefront Error Budget Summary

Mode: NGAO LGS
 Instrument: TBD
 Observation: KBO

	Science Band								
	u'	g'	r'	i'	Z	Y	J	H	K
λ (μm)	0.36	0.47	0.62	0.75	0.88	1.03	1.25	1.64	2.20
$\Delta\lambda$ (μm)	0.06	0.14	0.14	0.15	0.12	0.12	0.16	0.29	0.34
λ/D (mas)	7	10	13	15	18	21	26	34	46

High-order Errors (LGS Mode)	Wavefront Error (rms)	Parameter	Strehl Ratio (%)									
Atmospheric Fitting Error	41 nm	64 Subaps										
Bandwidth Error	26 nm	165 Hz (-3db)										
High-order Measurement Error	41 nm	150 W										
LGS Tomography Error	72 nm	8 bascon(s)										
Astigmatism Deformation Error	31 nm	0.50 m LLT										
Multiplexing Error	20 nm	18 zenith angle, H band										
Scintillation Error	15 nm	0.38 Scat index, H-band										
WFS Scintillation Error	10 nm	Alloc										
Uncorrectable Static Telescope Aberrations	43 nm	64 Acts										
Uncorrectable Dynamic Telescope Aberrations	11 nm	Dekeco Ph.D										
Static WFS Zero-point Calibration Error	25 nm	Alloc										
Dynamic WFS Zero-point Calibration Error	35 nm	Alloc										
Leaky Integrator Zero-point Calibration Error	15 nm	Alloc										
Go-to Control Errors	43 nm	Alloc										
Residual Na Layer Focus Change	20 nm	30 m/s Na layer vel										
DM Finite Stroke Errors	1 nm	4.0 um P-P stroke										
DM Hysteresis	13 nm	from TMT										
High-Order Aliasing Error	14 nm	64 Subaps										
DM Drive Digitization	1 nm	16 bits										
Uncorrectable AO System Aberrations	30 nm	Alloc										
Uncorrectable Instrument Aberrations	32 nm	TBD Instrument										
DM-to-lenslet Misregistration	15 nm	Alloc										
DM-to-lenslet Pupil Scale Error	15 nm	Alloc										
Angular Anisoplanatism Error	95 nm	5 arcsec										
Total High Order Wavefront Error	142 nm	172 nm	High Order Strehl	0.00	0.01	0.05	0.13	0.23	0.34	0.46	0.65	0.79

Tip/Tilt Errors	Angular Error (rms)	Equivalent WFE (rms)	Parameter	Strehl ratios (%)								
Tip Measurement Error (one-axis) <small>So Filter</small>	2.50 mas	44 nm	19.5 mag (mV)									
Tip Bandwidth Error (one-axis)	1.71 mas	29 nm	21.2 Hz									
Tip Anisoplanatism Error (one-axis)	2.84 mas	48 nm	34.9 arcsec									
Residual Centroid Anisoplanatism	0.95 mas	16 nm	10 x reduction									
Residual Atmospheric Dispersion <small>H</small>	0.14 mas	3 nm	20 x reduction									
Science Instrument Mechanical Drift	1.25 mas	36 nm	Alloc 0.25 mas / min									
Long Exposure Field Rotation Errors	2.50 mas	70 nm	Alloc 0.5 mas / min									
Residual Telescope Pointing Jitter (one-axis)	2.50 mas	42 nm	29 Hz input disturbance									
Total Tip/Tilt Error (one-axis)	5.7 mas	103 nm	Tip/Tilt Strehl	0.22	0.32	0.45	0.55	0.63	0.70	0.77	0.85	0.91

Total Effective Wavefront Error	199 nm	Total Strehl (%)	0.00	0.00	0.02	0.07	0.15	0.24	0.37	0.56	0.72
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Sky Coverage	Galactic Lat.	30 deg
Corresponding Sky Coverage	10.0%	This fraction of sky can be corrected to the Total Effective WFE shown

Assumptions / Parameters									
r0	0.175 m	at this zenith	Wind Speed	7.76 m/s	Zenith Angle	18 deg			
Theta0_eff	1.26 arcsec	at this zenith	Outer Scale	50 m	HO WFS Rate	2459 Hz	SH	using	CCID55
Sodium Abund.	4 x 10 ⁶	atoms/cm ²	LGS Ast. Rad.	0.52 arcmin	HO WFS Noise	2.7 e- rms			
Science Target	MOAO				HOWFS anti-aliasing	NO			
LOWFS Target	MOAO	Num TT 3	Num 3x3	0	LO WFS rate	550 Hz	SH	using	SNAP
LOWFS Star Type	M	Num TTFA 0	Num HOWFS	0	LO WFS Noise	4.5 e- rms			

Figure 2: + Wavefront error budget for Kuiper Belt Objects.

2.3 Exo Jupiter with LGS

An NGAO wavefront error budget for observations of exojupiters is shown in Figure 3. This observing scenario utilizes six laser beacons in an LTAO configuration. The science target is used as the tip tilt guide star, and is assumed to have $mV=13$. The H band Strehl ratio was optimized by allowing the parameters in Table 6 to float under the constraints indicated in this table. The optimizer chose a solution with the maximum allowed number of subapertures. For this $mV=13$ science target, the limiting 2.5 kHz tip tilt control loop rate was chosen by the solver. Optimizing the H band Strehl ratio generated a high order control loop rate of about 2 kHz and a laser asterism radius of .14 amin.

The dominant terms in the high order budget were errors from fitting, tomography, uncorrectable static telescope aberrations, and go-to control errors. The tip tilt error budget was dominated by tilt bandwidth error.

Variable Parameters	Subaperture width	$\geq .171$ m (≤ 64 subaps)
	High order integration time	No limit
	Tip tilt integration time	$\geq .0004$
	LGS asterism radius	No limit
Optimized Parameter	H band Strehl Ratio	74%

Table 6: Optimized parameter and constraints for the Exo Jupiter LGS observing scenario.

Keck Wavefront Error Budget Summary

Mode: NGAO LGS
 Instrument: TBD
 Observation: Exo Jup LGS

	Science Band								
	u'	g'	r'	i'	Z	Y	J	H	K
λ (μm)	0.36	0.47	0.62	0.75	0.88	1.03	1.25	1.64	2.20
$\delta\lambda$ (μm)	0.06	0.14	0.14	0.15	0.12	0.12	0.16	0.29	0.34
λ/D (mas)	7	10	13	15	18	21	26	34	46

High-order Errors (LGS Mode)	Wavefront Error (rms)	Parameter	Strehl Ratio (%)									
Atmospheric Fitting Error	41 nm	64 Subaps										
Bandwidth Error	29 nm	138 Hz (-3db)										
High-order Measurement Error	35 nm	150 W										
LGS Tomography Error	43 nm	6 beacon(s)										
Asternism Deformation Error	29 nm	0.50 m LLT										
Multiplex Error	19 nm	10 zenith angle, H band										
Scintillation Error	14 nm	0.36 Scat index, H-band										
WFS Scintillation Error	10 nm	Alicc										
Uncorrectable Static Telescope Aberrations	43 nm	64 Acts										
Uncorrectable Dynamic Telescope Aberrations	13 nm	Dekans Ph.D										
Static WFS Zero-point Calibration Error	25 nm	Alicc										
Dynamic WFS Zero-point Calibration Error	35 nm	Alicc										
Leaky Integrator Zero-point Calibration Error	15 nm	Alicc										
Go-to Control Errors	43 nm	Alicc										
Residual Na Layer Focus Change	19 nm	30 m/s Na layer vel										
DM Finite Stroke Errors	1 mm	4.0 um P-P stroke										
DM Hysteresis	13 nm	from TMT										
High-Order Aliasing Error	14 nm	64 Subaps										
DM Drive Digitization	1 mm	16 bits										
Uncorrectable AO System Aberrations	30 nm	Alicc										
Uncorrectable Instrument Aberrations	30 nm	TBD Instrument										
DM-to-lenslet Misregistration	15 nm	Alicc										
DM-to-lenslet Pupil Scale Error	15 nm	Alicc										
Angular Anisoplanatism Error	94 nm	1 arcsec										
Total High Order Wavefront Error	127 nm	129 nm	High Order Strehl	0.01	0.06	0.19	0.32	0.44	0.55	0.67	0.79	0.88

Tip/Tilt Errors	Angular Error (rms)	Equivalent WFE (rms)	Parameter	Strehl ratios (%)								
Tilt Measurement Error (one-axis)	0.18 mas	3 nm	13.0 mag (mV)									
Tilt Bandwidth Error (one-axis)	0.06 mas	16 nm	38.5 Hz									
Tilt Anisoplanatism Error (one-axis)	0.00 mas	0 nm	0.0 arcsec									
Residual Centroid Anisoplanatism	0.03 mas	16 nm	10 x reduction									
Residual Atmospheric Dispersion	0.08 mas	1 mm	20 x reduction									
Science Instrument Mechanical Drift	1.25 mas	36 nm	Alicc 0.25 mas / min									
Long Exposure Field Rotation Errors	2.50 mas	70 nm	Alicc 0.5 mas / min									
Residual Telescope Pointing Jitter (one-axis)	1.38 mas	23 nm	29 Hz input disturbance									
Total Tip/Tilt Error (one-axis)	3.4 mas	63 nm	Tip/Tilt Strehl	0.44	0.58	0.70	0.78	0.83	0.87	0.91	0.94	0.97

Total Effective Wavefront Error	141 nm	Total Strehl (%)	0.00	0.03	0.13	0.25	0.37	0.48	0.61	0.74	0.85
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Sky Coverage	Galactic Lat.	30 deg
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Corresponding Sky Coverage	0.0%	This fraction of sky can be corrected to the Total Effective WFE shown
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Assumptions / Parameters											
r0	0.178 m	at this zenith	Wind Speed	7.93 m/s	Zenith Angle	10 deg					
Theta0_eff	1.33 arcsec	at this zenith	Outer Scale	50 m	HO WFS Rate	2071 Hz	SH	using	CCID66		
Sodium Abund.	4 x 10 ⁸	atoms/cm ²	LGS Ast. Rad.	0.14 arcmin	HO WFS Noise	2.5 e- rms					
Science Target:	MOAO				HOWFS anti-aliasing	NO					
LOWFB Target:	MOAO	Num TT 3	Num 3a3	0	LO WFS rate	2500 Hz	SH	using	SNAP		
LOWFB Star Type:	M	Num TTFA 0	Num HDWFS	0	LO WFS Noise	4.5 e- rms					

Figure 3: Wavefront error budget for Exo Jupiter LGS.

2.4 Extended Groth Strip

An NGAO wavefront error budget for galactic observations in the extended Groth strip is shown in Figure 4. This observing scenario uses six laser beacons in an MOAO or LTAO configuration. Optimization of the H band Strehl ratio yields a high order update rate of 2.25 kHz, the maximum allowed number of subapertures, and a laser asterism radius of .8 amin.

The requirement of 30% sky coverage yields a limiting tip tilt guide star magnitude of $m_V=20.4$, with a tip tilt guide star search radius of 50 asec and a tip tilt update rate of 400 Hz.

For this science case, the high order budget is dominated by tomography error. Due to the long integration times required in this observing scenario, the tilt error budget is dominated by mechanical drift and field rotation errors.

Variable Parameters	High order integration time	No Limit
	Subaperture width	$\geq .171$ m (≤ 64 subaps)
	Tip tilt integration time	No Limit
	Tip tilt guide star search radius	No Limit
	LGS asterism radius	No Limit
	Sky Coverage	=30%
Optimized Parameter	H band Strehl Ratio	36%

Table 7: Optimized parameter and constraints for the Extended Groth Strip observing scenario.

Keck Wavefront Error Budget Summary

Mode: NGAO LGS
 Instrument: TBD
 Observation: Extended Groth Strip

	Science Band								
	u'	g'	r'	i'	Z	Y	J	H	K
λ (μm)	0.36	0.47	0.62	0.75	0.88	1.03	1.25	1.64	2.20
$\delta\lambda$ (μm)	0.06	0.14	0.14	0.15	0.12	0.12	0.16	0.29	0.34
λ/D (mas)	7	10	13	15	18	21	26	34	46

High-order Errors (LGS Mode)	Wavefront Error (rms)	Parameter	Strehl Ratio (%)
Atmospheric Fitting Error	44 nm	64 Subap	
Bandwidth Error	30 nm	151 Hz (-3db)	
High-order Measurement Error	45 nm	150 W	
LGS Tomography Error	89 nm	6 beacon(s)	
Asterism Deformation Error	38 nm	0.50 m LLT	
Multispectral Error	23 nm	34 zenith angle, H band	
Scintillation Error	20 nm	0.49 Scat index, H-band	
WFS Scintillation Error	10 nm	Alloc	
Uncorrectable Static Telescope Aberrations	43 nm	64 Acts	
Uncorrectable Dynamic Telescope Aberrations	12 nm	Dekans Ph.D	
Static WFS Zero-point Calibration Error	25 nm	Alloc	
Dynamic WFS Zero-point Calibration Error	35 nm	Alloc	
Leaky Integrator Zero-point Calibration Error	15 nm	Alloc	
Go-to Control Errors	43 nm	Alloc	
Residual Na Layer Focus Change	23 nm	30 m/s Na layer vel	
DM Finite Stroke Errors	1 nm	4.0 um P-P stroke	
DM Hysteresis	13 nm	from TMT	
High-Order Aliasing Error	15 nm	64 Subap	
DM Drive Digitization	1 nm	16 bits	
Uncorrectable AD System Aberrations	30 nm	Alloc	
Uncorrectable Instrument Aberrations	30 nm	TBD Instrument	
DM-to-lenslet Misregistration	15 nm	Alloc	
DM-to-lenslet Pupil Scale Error	15 nm	Alloc	
Angular Anisoplanatism Error	95 nm	43 nm	1.5 arcsec

Total High Order Wavefront Error	156 nm	162 nm	High Order Strehl	0.00	0.01	0.07	0.16	0.27	0.39	0.52	0.69	0.81
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Tip/Tilt Errors	Angular Error (rms)	Equivalent WFE (rms)	Parameter	Strehl ratios (%)
Tilt Measurement Error (one-axis) <small>Sci Filter</small>	4.58 mas	77 nm	20.4 mag (mV)	
Tilt Bandwidth Error (one-axis)	1.92 mas	33 nm	17.6 Hz	
Tilt Anisoplanatism Error (one-axis)	4.37 mas	74 nm	50.2 arcsec	
Residual Centroid Anisoplanatism	1.02 mas	17 nm	10 x reduction	
Residual Atmospheric Dispersion <small>K</small>	0.14 mas	3 nm	20 x reduction	
Science Instrument Mechanical Drift	7.50 mas	250 nm	Alloc 0.25 mas / min	
Long Exposure Field Rotation Errors	15.00 mas	309 nm	Alloc 0.5 mas / min	
Residual Telescope Pointing Jitter (one-axis)	3.01 mas	51 nm	29 Hz input disturbance	

Total Tip/Tilt Error (one-axis)	18.3 mas	288 nm	Tip/Tilt Strehl	0.03	0.04	0.08	0.11	0.14	0.19	0.25	0.36	0.51
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Total Effective Wavefront Error		329 nm	Total Strehl (%)	0.00	0.00	0.01	0.02	0.04	0.07	0.13	0.25	0.41
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Sky Coverage	Galactic Lat.	30 deg
Corresponding Sky Coverage		30.0%

This fraction of sky can be corrected to the Total Effective WFE shown

Assumptions / Parameters											
r0	0.151 m	at this zenith	Wind Speed	7.15 m/s	Zenith Angle	34 deg					
Theta0_eff	1.01 arcsec	at this zenith	Outer Scale	50 m	HO WFS Rate	2265 Hz	SH	using	CCID65		
Sodium Abund.	4 x 10 ⁶	atoms/cm ²	LGS Ast. Rad.	0.80 arcmin	HO WFS Noise	2.6 e- rms					
Science Target:	MOAO				HOWFS anti-aliasing	NO					
LOWFS Target:	MOAO	Num TT 3	Num 3x3	0	LO WFS rate	407 Hz	SH	using	SNAP		
LOWFS Star Type:	M	Num TTPA 0	Num HOWFS	0	LO WFS Noise	4.5 e- rms					

Figure 4: Wavefront error budget for Extended Groth Strip observing scenario.

2.5 Galactic Center

An NGAO wavefront error budget for observations of the galactic center is shown in Figure 5. This observing scenario uses an 6 beacons in an LTAO architecture, and employs the known tip tilt guide star IRS7. Maximizing the H band Strehl ratio yields a high order update rate of 1.7 kHz, 64 subapertures, and an asterism radius of .13 amin. The budget employs the maximum allowed tip tilt update rate of 2.5 kHz.

For this scenario, the high order budget is dominated by angular anisoplanatism across the 10 asec field. Tip tilt errors are negligably small in this case. The 36% H band Strehl ratio corresponds to system performance at the corner of the 10 asec field.

Variable Parameters	High order integration time	No Limit
	Subaperture width	$\geq .171$ m (≤ 64 subaps)
	Tip tilt integration time	$\geq .0004$ sec
	LGS asterism radius	No Limit
Optimized Parameter	H band Strehl Ratio	36%

Table 8: Optimized parameter and constraints for the Galactic Center observing scenario.

Keck Wavefront Error Budget Summary

Mode: NGAO LGS
 Instrument: NIRC2
 Observation: Gal Cen

	Science Band								
	u'	g'	r'	i'	Z	Y	J	H	K
λ (μm)	0.36	0.47	0.62	0.75	0.88	1.03	1.25	1.64	2.20
$\delta\lambda$ (μm)	0.06	0.14	0.14	0.15	0.12	0.12	0.16	0.29	0.34
λ/D (mas)	7	10	13	15	18	21	26	34	46

High-order Errors (LGS Mode)	Wavefront Error (rms)	Parameter	Strehl Ratio (%)
Atmospheric Fitting Error	48 nm	64 Subap	
Bandwidth Error	41 nm	113 Hz (-3dB)	
High-order Measurement Error	48 nm	150 W	
LGS Tomography Error	41 nm	6 beacon(s)	
Astigmatism Deformation Error	51 nm	0.50 m LLT	
Multispectral Error	27 nm	46 zenith angle, H band	
Scintillation Error	27 nm	0.68 Scat index, H-band	
WFS Scintillation Error	10 nm	Alloc	
Uncorrectable Static Telescope Aberrations	43 nm	64 Acts	
Uncorrectable Dynamic Telescope Aberrations	15 nm	DeKans Ph.D	
Static WFS Zero-point Calibration Error	25 nm	Alloc	
Dynamic WFS Zero-point Calibration Error	35 nm	Alloc	
Lesky Integrator Zero-point Calibration Error	15 nm	Alloc	
Go-to Control Errors	43 nm	Alloc	
Residual Na Layer Focus Change	28 nm	30 m/s Na layer vel	
DM Finite Stroke Errors	1 nm	4.0 μm P-P stroke	
DM Hysteresis	13 nm	from TMT	
High-Order Aliasing Error	16 nm	64 Subap	
DM Drive Digitization	1 nm	16 bits	
Uncorrectable AO System Aberrations	30 nm	Alloc	
Uncorrectable Instrument Aberrations	110 nm	NIRC2 instrument	
DM-to-lenslet Misregistration	15 nm	Alloc	
DM-to-lenslet Pupil Scale Error	15 nm	Alloc	
Angular Anisoplanatism Error	144 nm	7.1 arcsec	
Total High Order Wavefront Error	181 nm	268 nm	High Order Strehl 0.00 0.00 0.00 0.01 0.03 0.07 0.16 0.35 0.56

Tip/Tilt Errors	Angular Error (rms)	Equivalent WFE (rms)	Parameter	Strehl ratios (%)
Til Measurement Error (one-axis) Sci Filter	0.11 mas	2 nm	12.2 mag (mV)	
Til Bandwidth Error (one-axis)	0.81 mas	14 nm	38.5 Hz	
Til Anisoplanatism Error (one-axis)	0.52 mas	9 nm	5.5 arcsec	
Residual Control Anisoplanatism	1.11 mas	19 nm	10 \times reduction	
Residual Atmospheric Dispersion K	0.22 mas	4 nm	20 \times reduction	
Science Instrument Mechanical Drift	0.13 mas	5 nm	Alloc 0.25 mas / min	
Long Exposure Field Rotation Errors	0.25 mas	10 nm	Alloc 0.5 mas / min	
Residual Telescope Pointing Jitter (one-axis)	1.38 mas	23 nm	29 Hz input disturbance	
Total Tip/Tilt Error (one-axis)	2.0 mas	38 nm	Tip/Tilt Strehl 0.68 0.79 0.87 0.91 0.93 0.95 0.96 0.98 0.99	

Total Effective Wavefront Error	271 nm	Total Strehl (%) 0.00 0.00 0.00 0.01 0.02 0.07 0.16 0.34 0.56
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Sky Coverage Galactic Lat. 30 deg
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Corresponding Sky Coverage 0.2%	This fraction of sky can be corrected to the Total Effective WFE shown
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Assumptions / Parameters							
r0	0.145 m	at this zenith	Wind Speed	6.43 m/s	Zenith Angle	46 deg	
Theta0_off	0.76 arcsec	at this zenith	Outer Scale	50 m	HO WFS Rate	1702 Hz	BH using CCID66
Sodium Abund.	4×10^6	atoms/cm ²	LGS Ast. Rad.	0.13 arcmin	HO WFS Noise	2.2 e- rms	
Science Target:	MCOAO				HOWFS anti-aliasing	NO	
LOWFS Target:	MCOAO	Num TT 3	Num 3x3	0	LO WFS rate	2500 Hz	BH using SNAP
LOWFS Star Type:	IRS7	Num TTFA 0	Num HOWFS	0	LO WFS Noise	4.5 e- rms	

Figure 5: Wavefront error budget for the Galactic Center observing scenario.

3 Summary

This report summarizes the system performance predicted by the wavefront error budget spreadsheet for the five science cases considered in the NGAO study.